

ae senior thesis

april 26, 2013

advisor: dr. boothby

victoria interval [struc]



# MTOB

( multi-tenant  
office building )

pennsylvania



ae senior thesis

april 26, 2013

advisor: dr. boothby

victoria interval [struc]



# MTOB

( multi-tenant  
office building )

pennsylvania

introduction  
proposal  
redesign  
mechanical  
architectural  
conclusion



# stats

152,000 SF

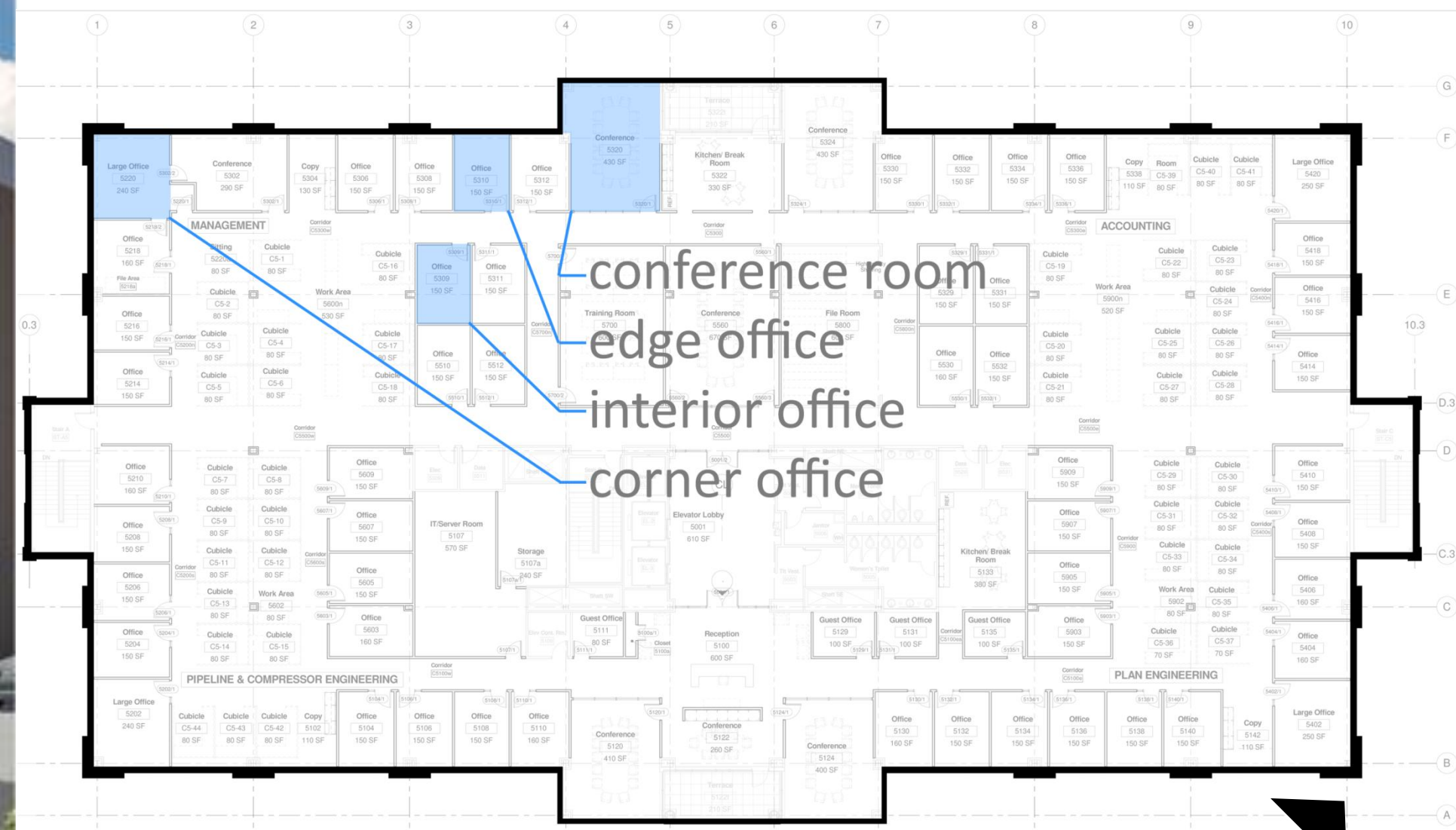
5 stories

composite steel framing

construction July 2012 to July 2013

located in office park

introduction  
 proposal  
 redesign  
 mechanical  
 architectural  
 conclusion





# project team

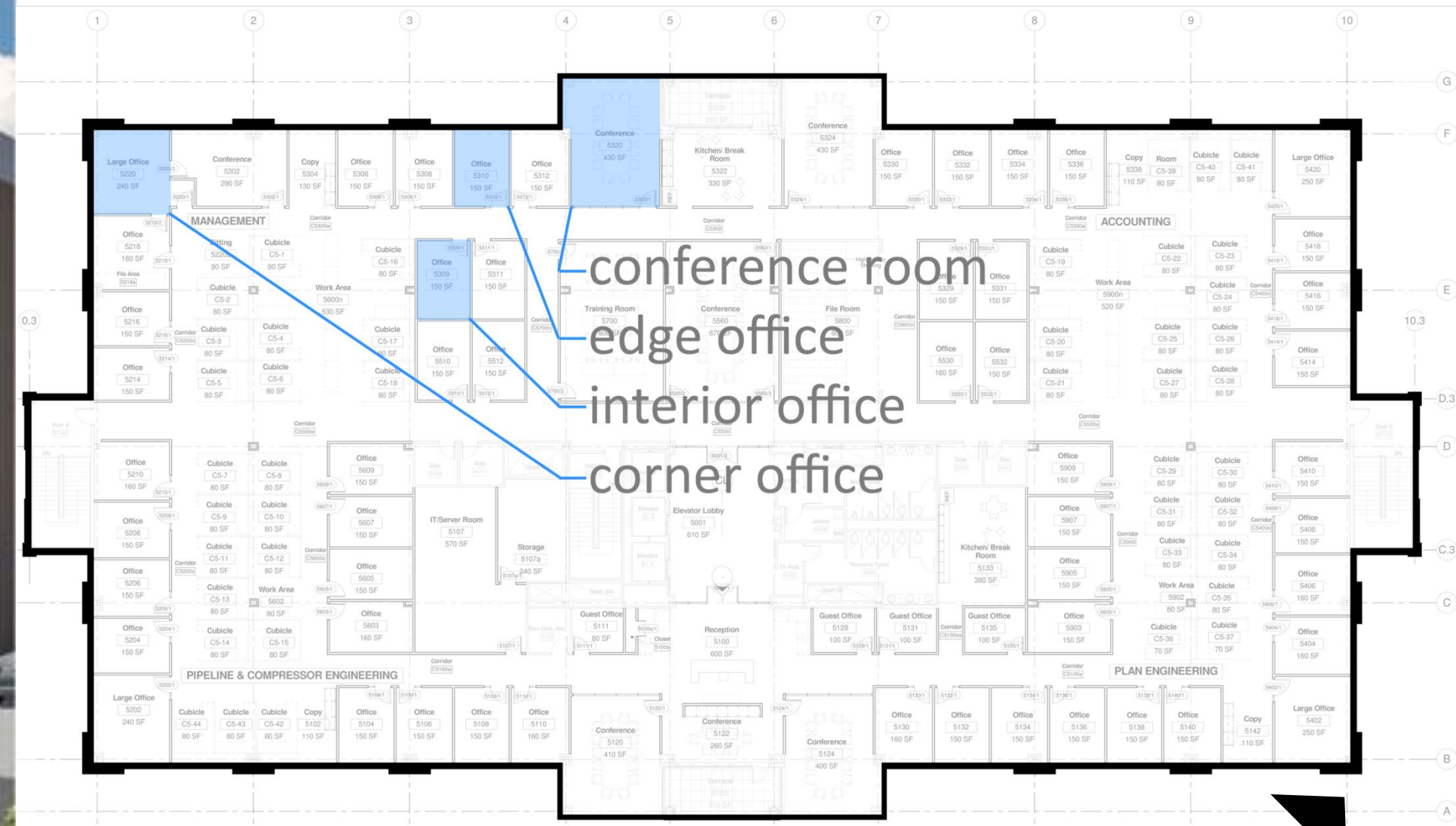
general contractor | **Rycon Construction**  
Construction Inc.

architect | **Kernick Architecture, LLC**

structural engr | **Atlantic Engineering Services**

site/civil engr | **Gateway Engineers**  
On Call. On Time. On Target.

introduction  
proposal  
redesign  
mechanical  
architectural  
conclusion

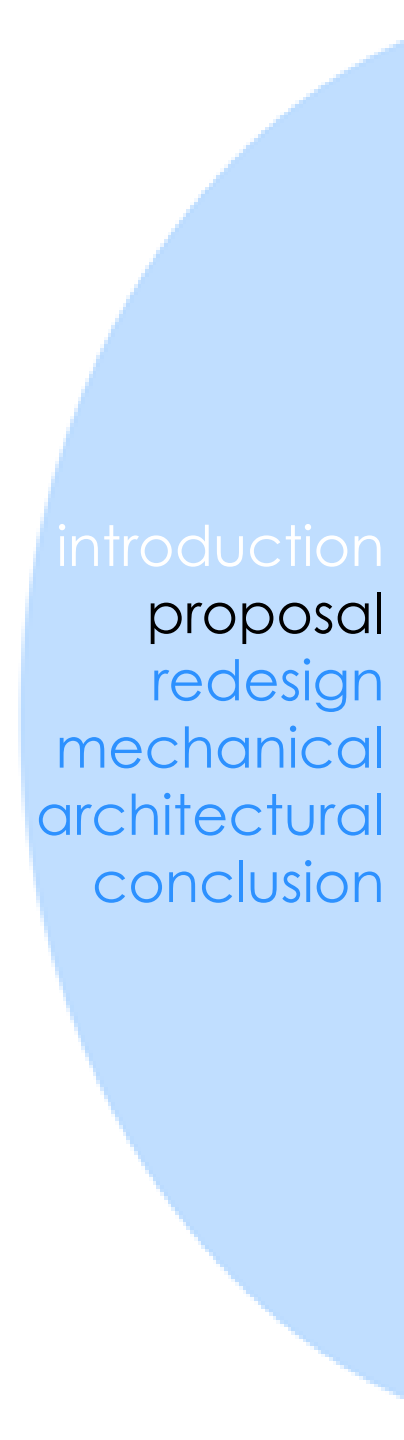


# scenario

tenant looking for more **contemporary** high-end space:

**open** feel

**modern** materials



introduction  
proposal  
redesign  
mechanical  
architectural  
conclusion

# scenario

# proposal



tenant looking for more **contemporary** high-end space:

**open** feel

**modern** materials

→ **struc** – cellular beams in exposed ceiling

introduction  
proposal  
redesign  
mechanical  
architectural  
conclusion

# scenario

# proposal

tenant looking for more **contemporary** high-end space:

**open** feel

**modern** materials

→ **struc** – cellular beams in exposed ceiling

→ **mech** – run through structure (IBC height restriction)

introduction  
proposal  
redesign  
mechanical  
architectural  
conclusion



# scenario

# proposal

tenant looking for more **contemporary** high-end space:

**open** feel

**modern** materials

→ **struc** – cellular beams in exposed ceiling

→ **arch** – façade redesign (aesthetics + thermal)

→ **mech** – run through structure (IBC height restriction)

introduction  
proposal  
redesign  
mechanical  
architectural  
conclusion

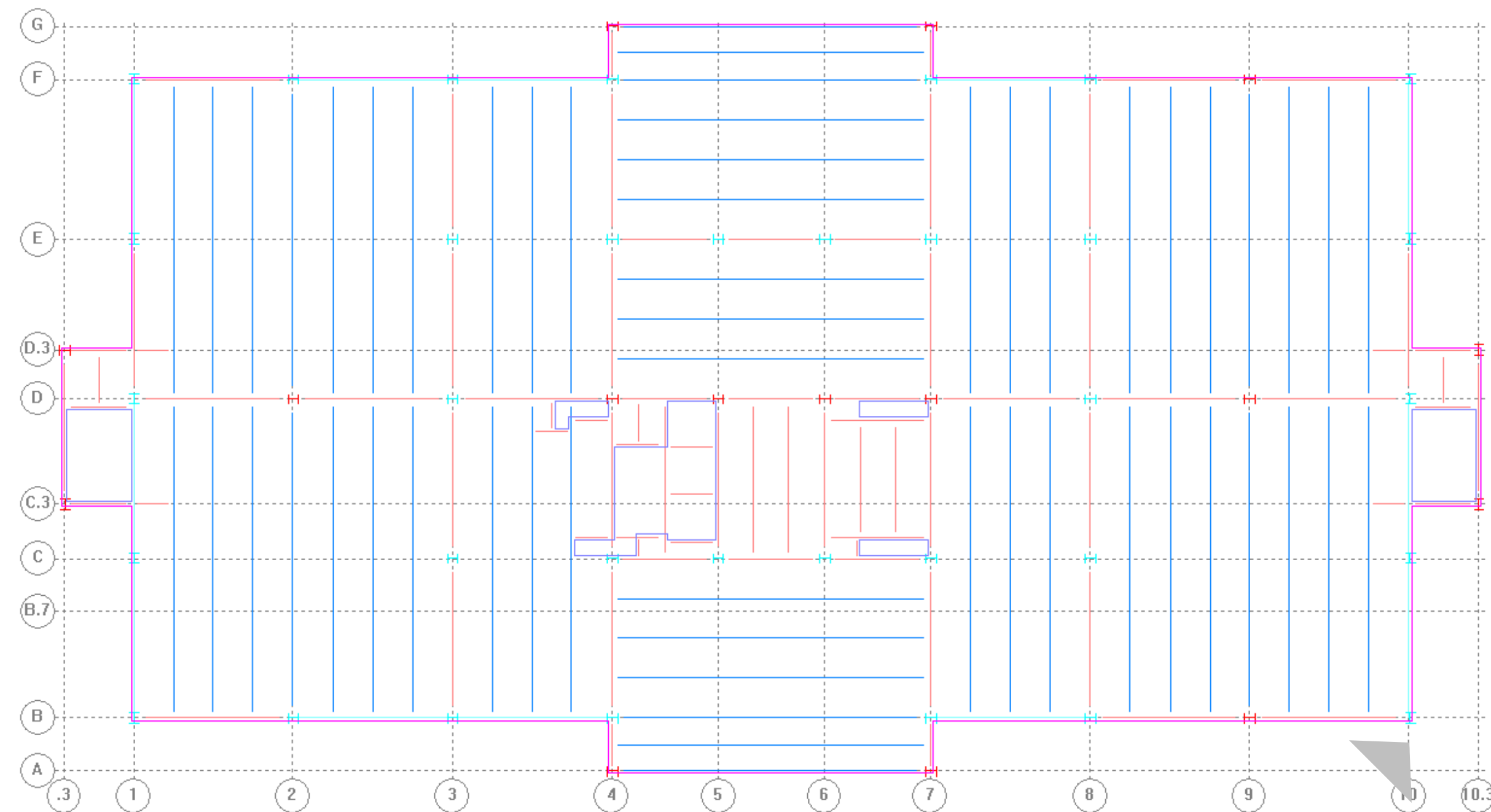
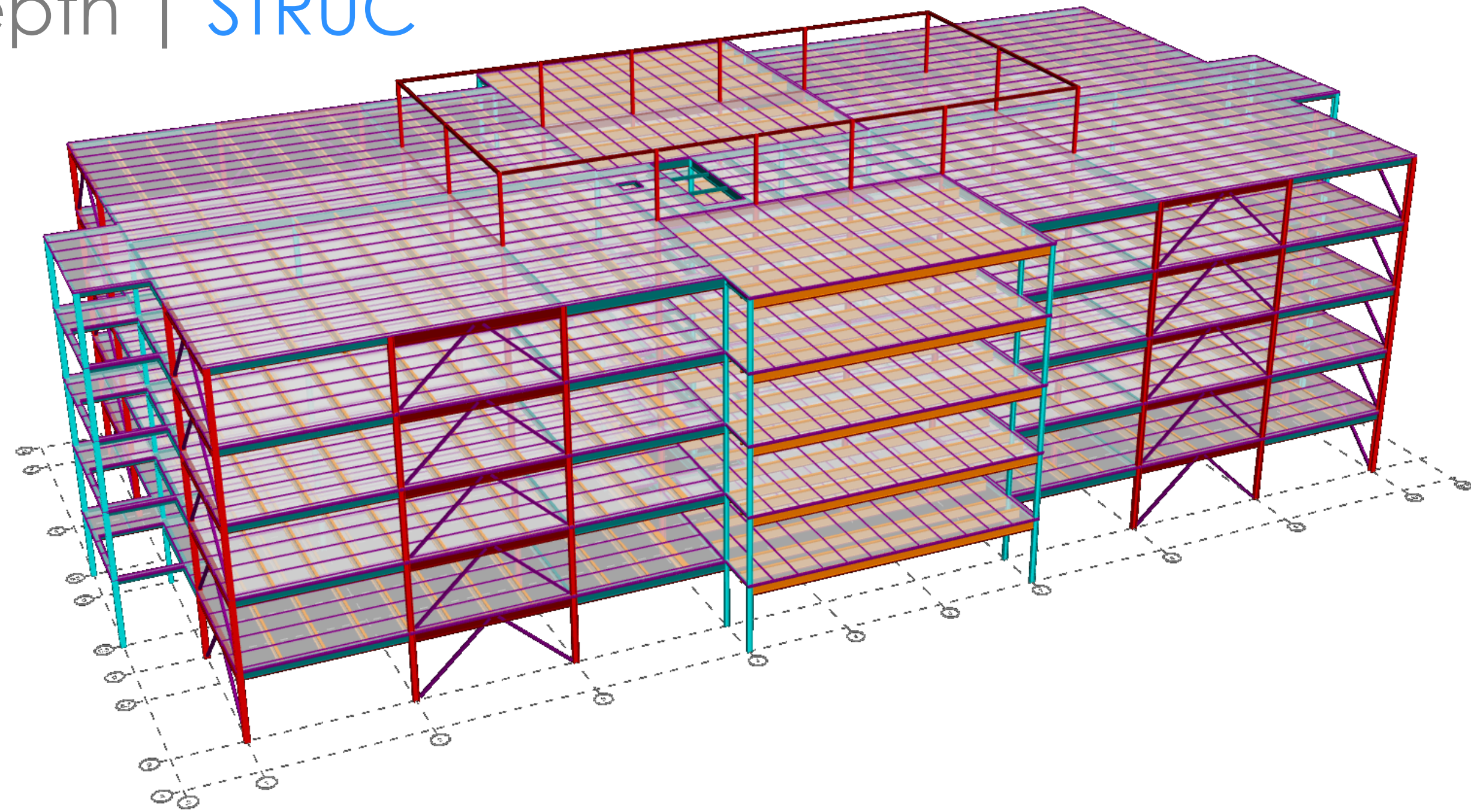






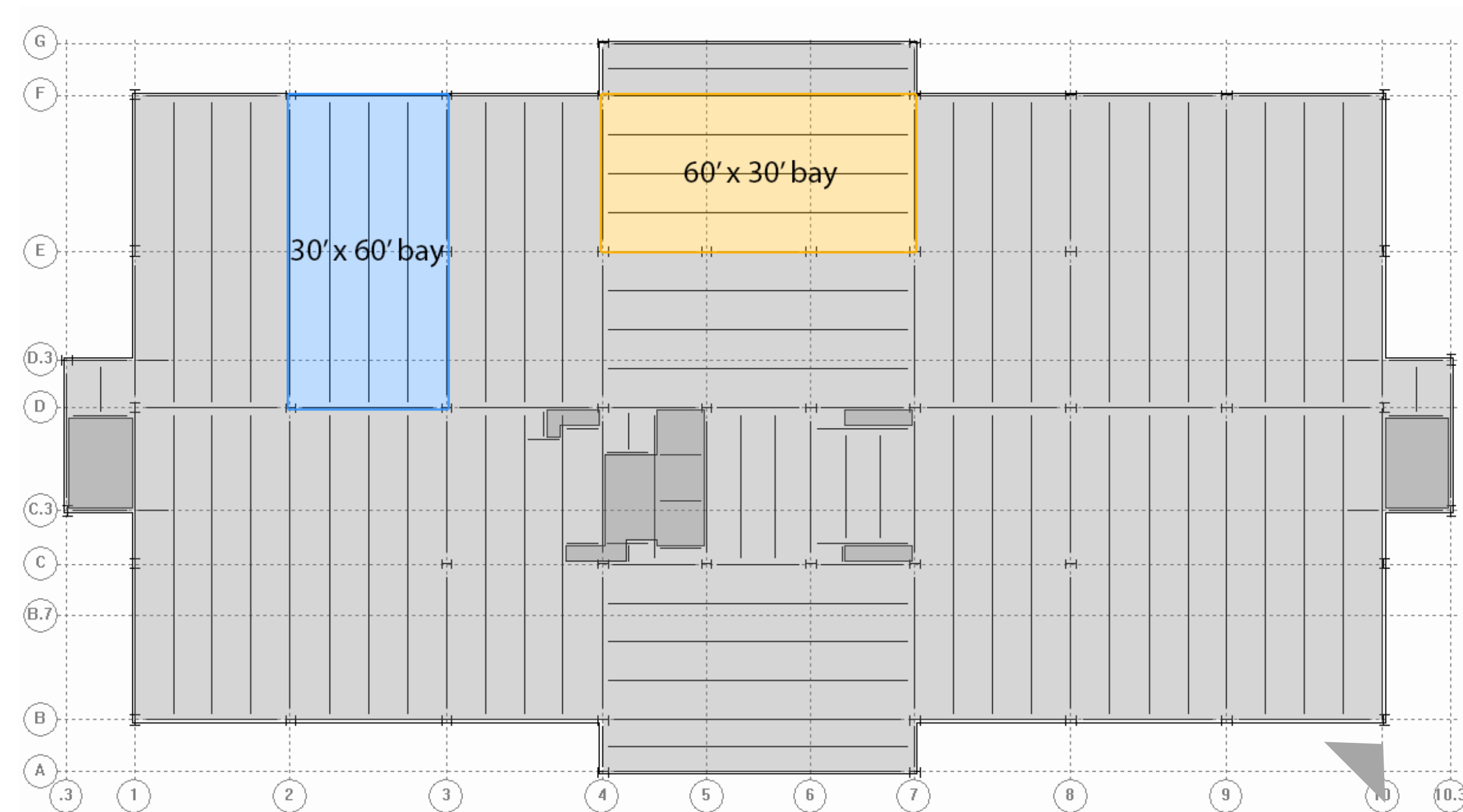
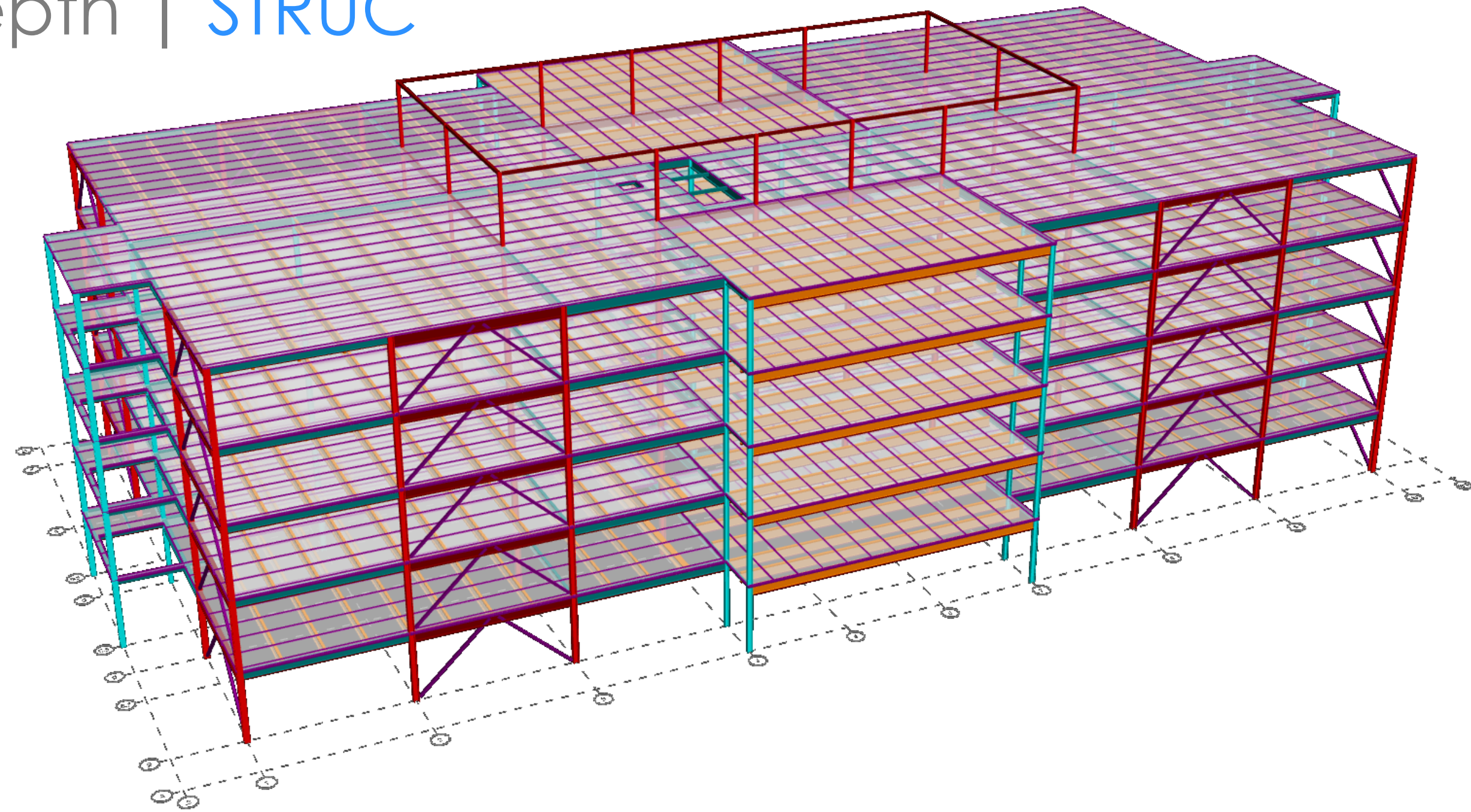
introduction  
proposal  
redesign  
mechanical  
architectural  
conclusion

# depth | STRUC



introduction  
proposal  
redesign  
mechanical  
architectural  
conclusion

# depth | STRUC

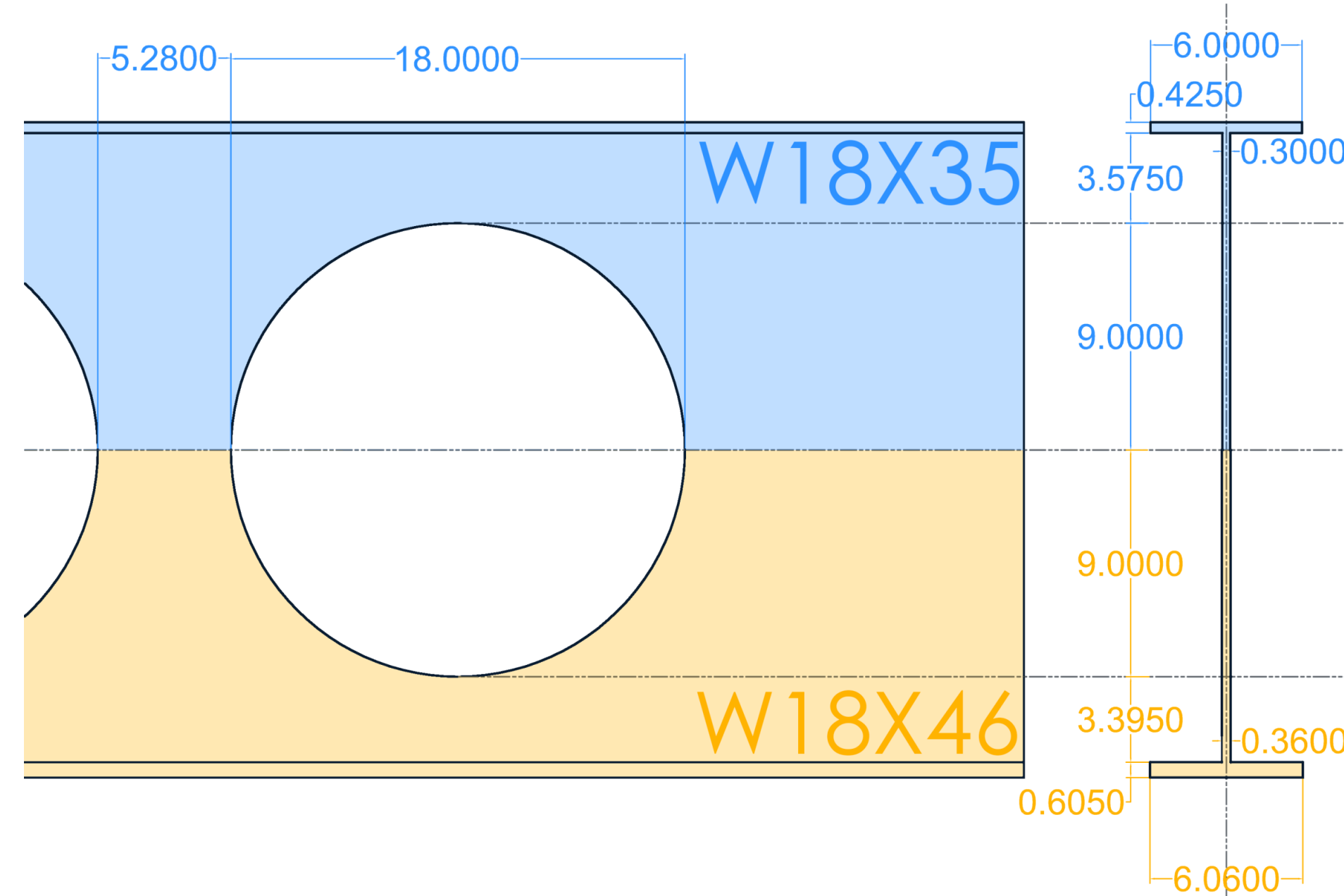


introduction  
proposal  
redesign  
mechanical  
architectural  
conclusion



RAM optimized:

LB27x35/46

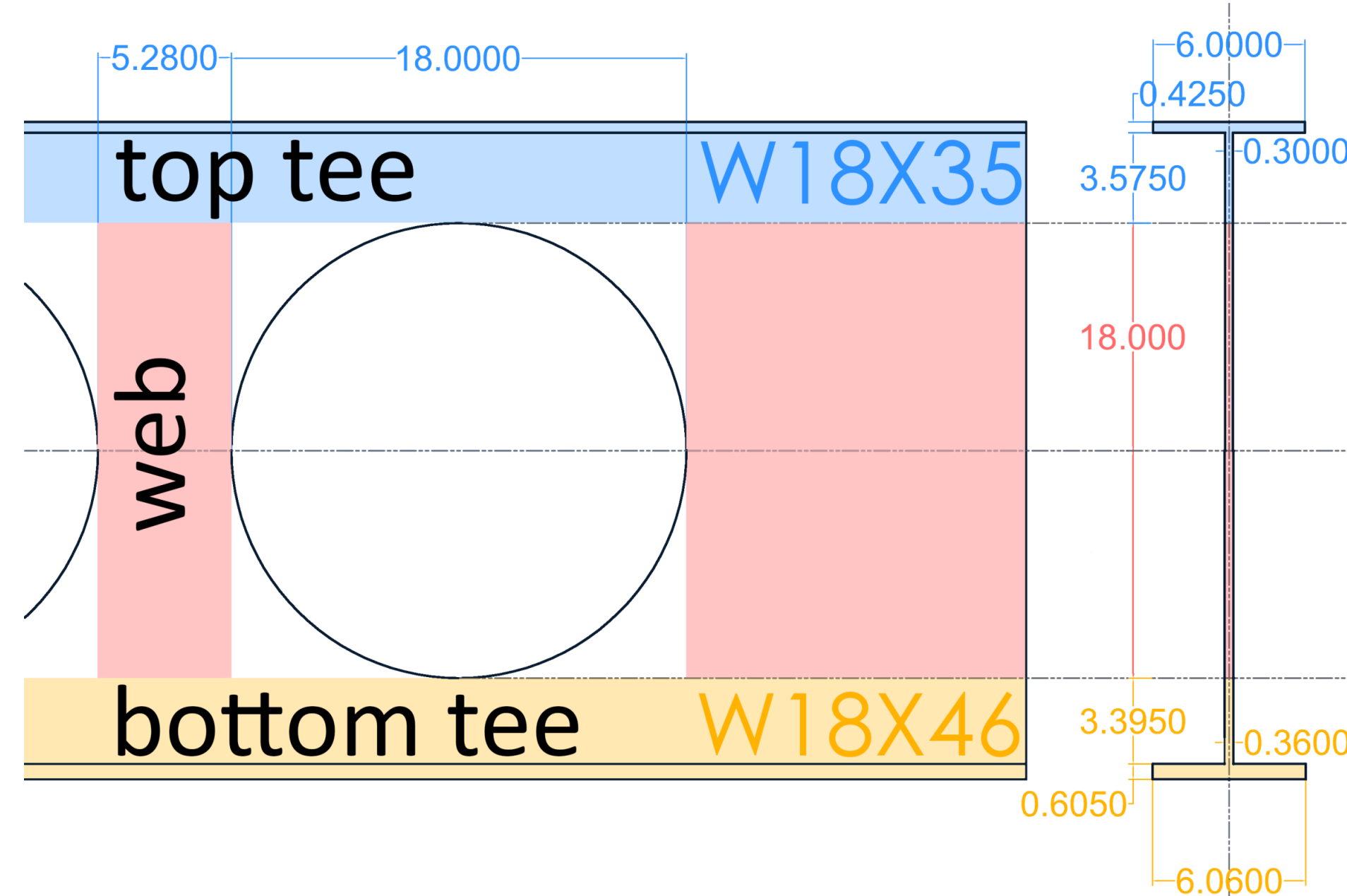


introduction  
proposal  
redesign  
mechanical  
architectural  
conclusion



RAM optimized:

LB27x35/46

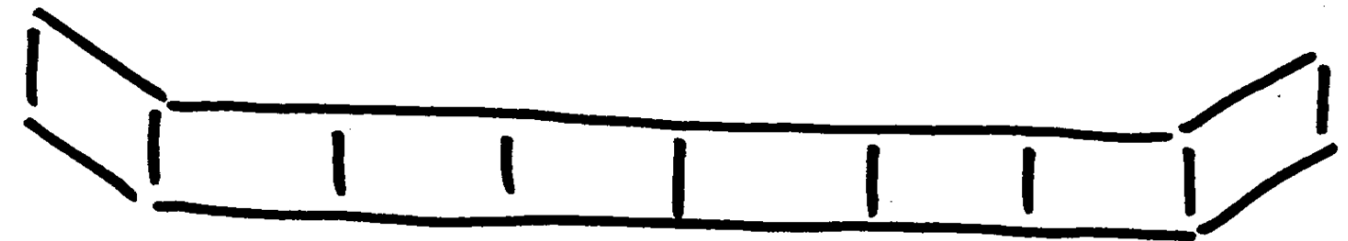
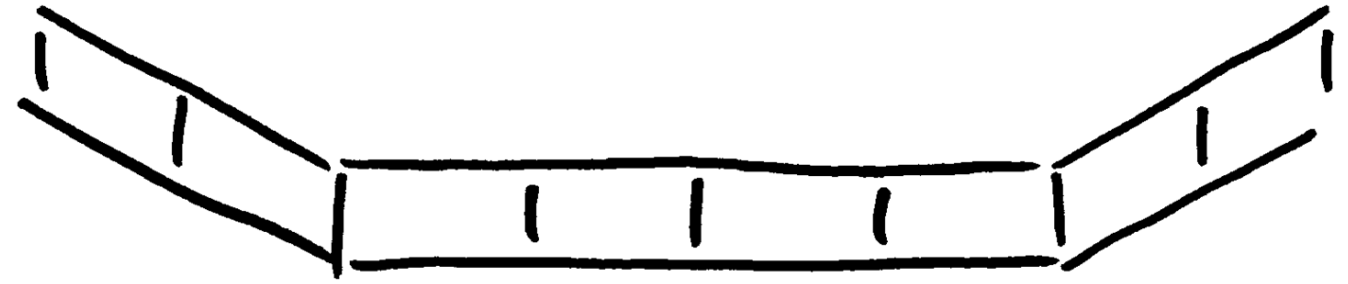
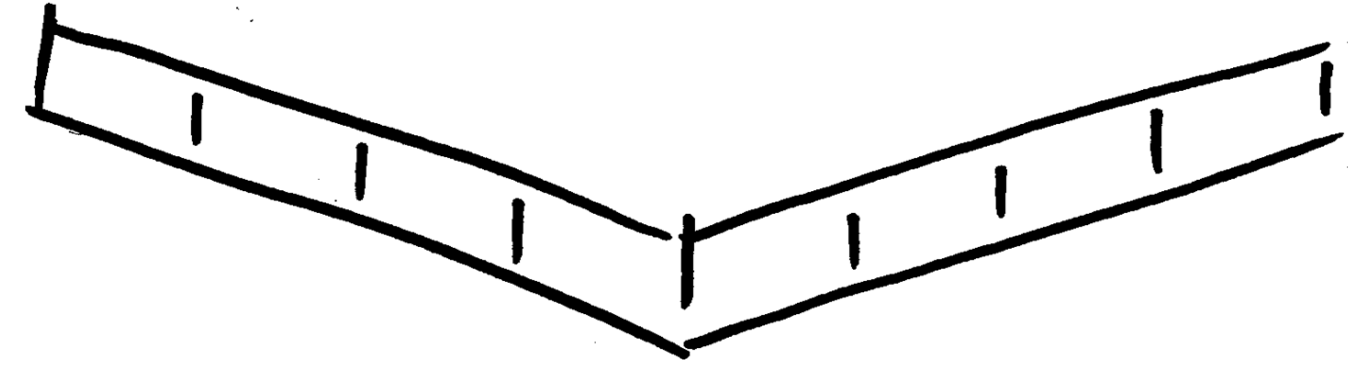


## plastic analysis assumptions

- + behaves like Vierendeel Truss
- + failure mechanism will be symmetrical

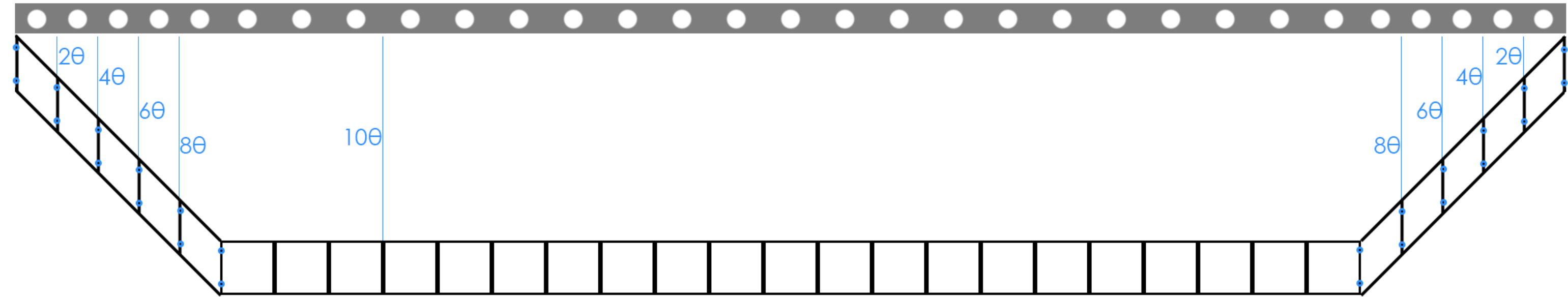
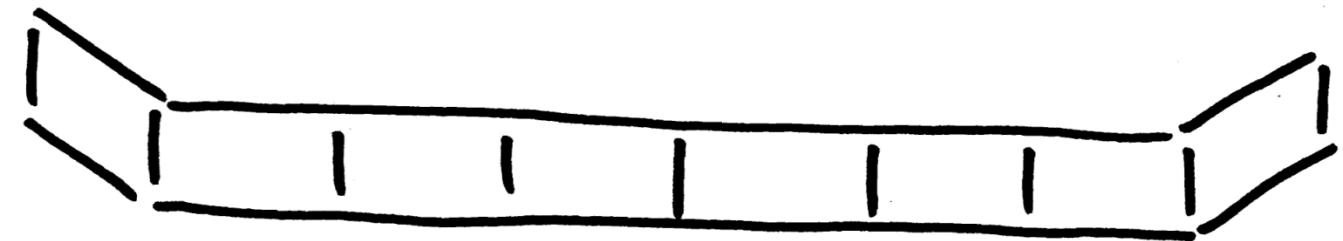
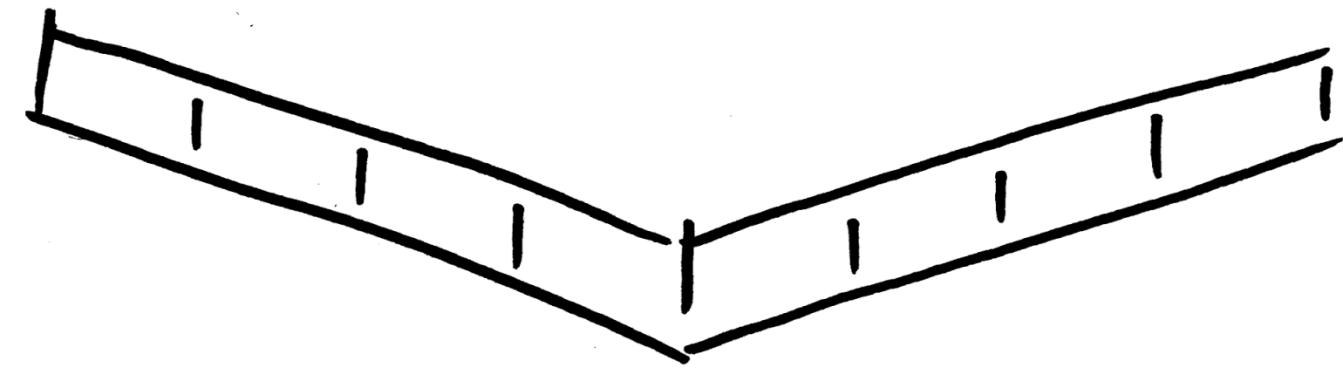
introduction  
proposal  
redesign  
mechanical  
architectural  
conclusion

# depth | STRUC plastic analysis



introduction  
proposal  
redesign  
mechanical  
architectural  
conclusion

# depth | STRUC plastic analysis



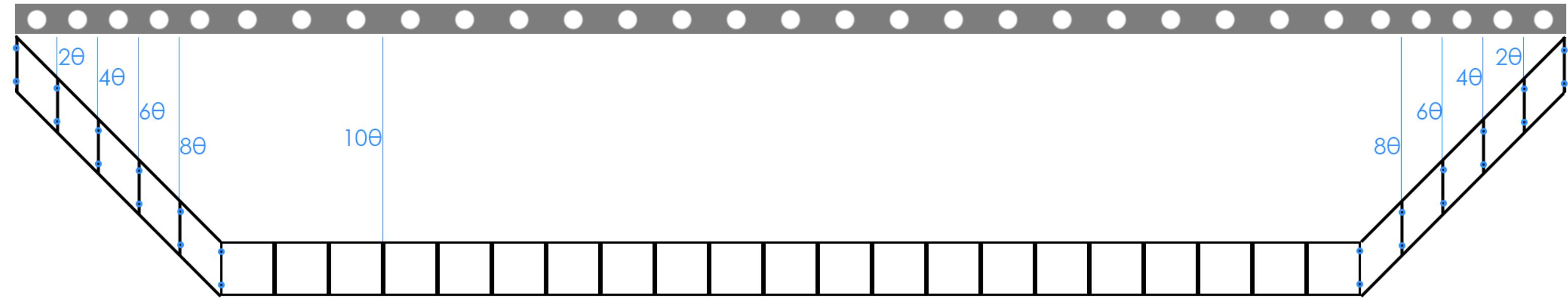
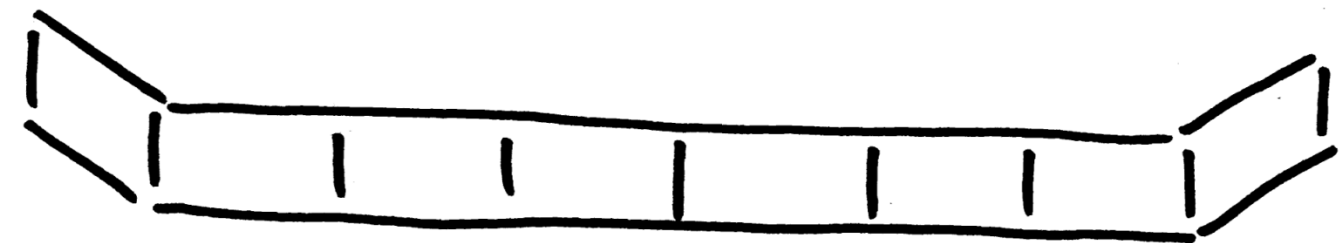
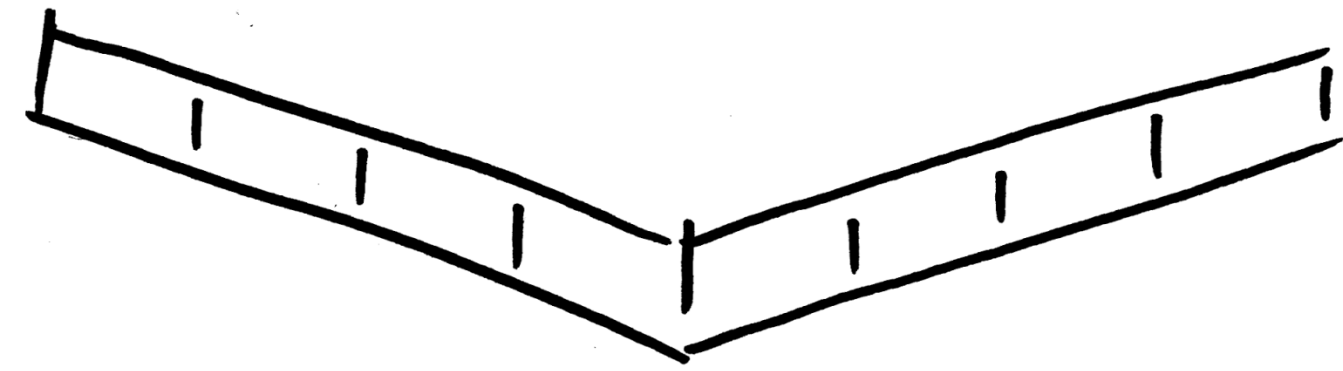
controlling collapse mechanism

failure load  $P = 11 \text{ k} = 5.5 \text{ klf}$

actual load = 0.9 klf

introduction  
proposal  
redesign  
mechanical  
architectural  
conclusion

# depth | STRUC plastic analysis



controlling collapse mechanism

failure load  $P = 11 k = 5.5 \text{ klf}$

actual load = 0.9 klf

+ axial force in flanges

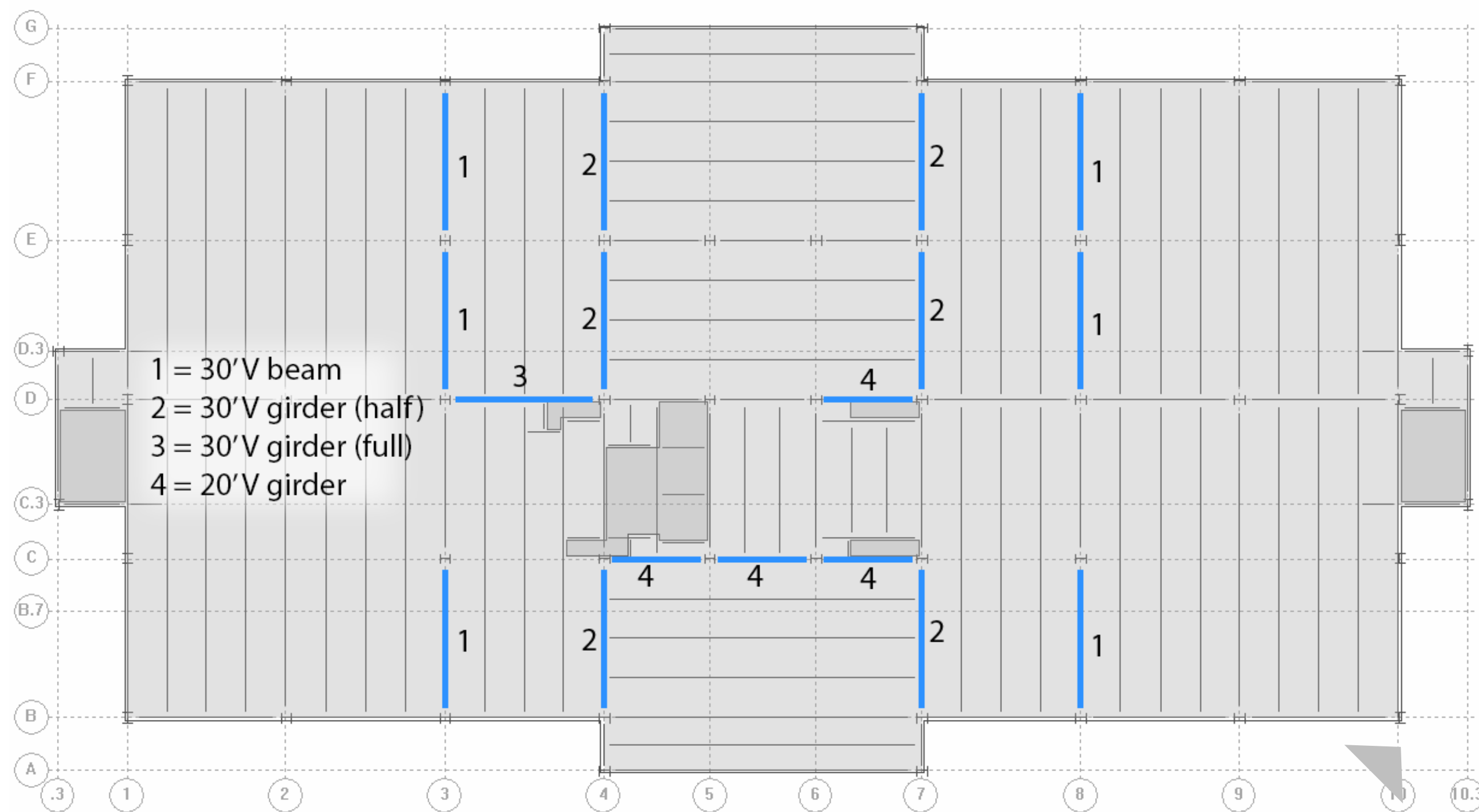
+ deflection

+ web buckling

introduction  
proposal  
redesign  
mechanical  
architectural  
conclusion



# depth | STRUC vierendeel trusses

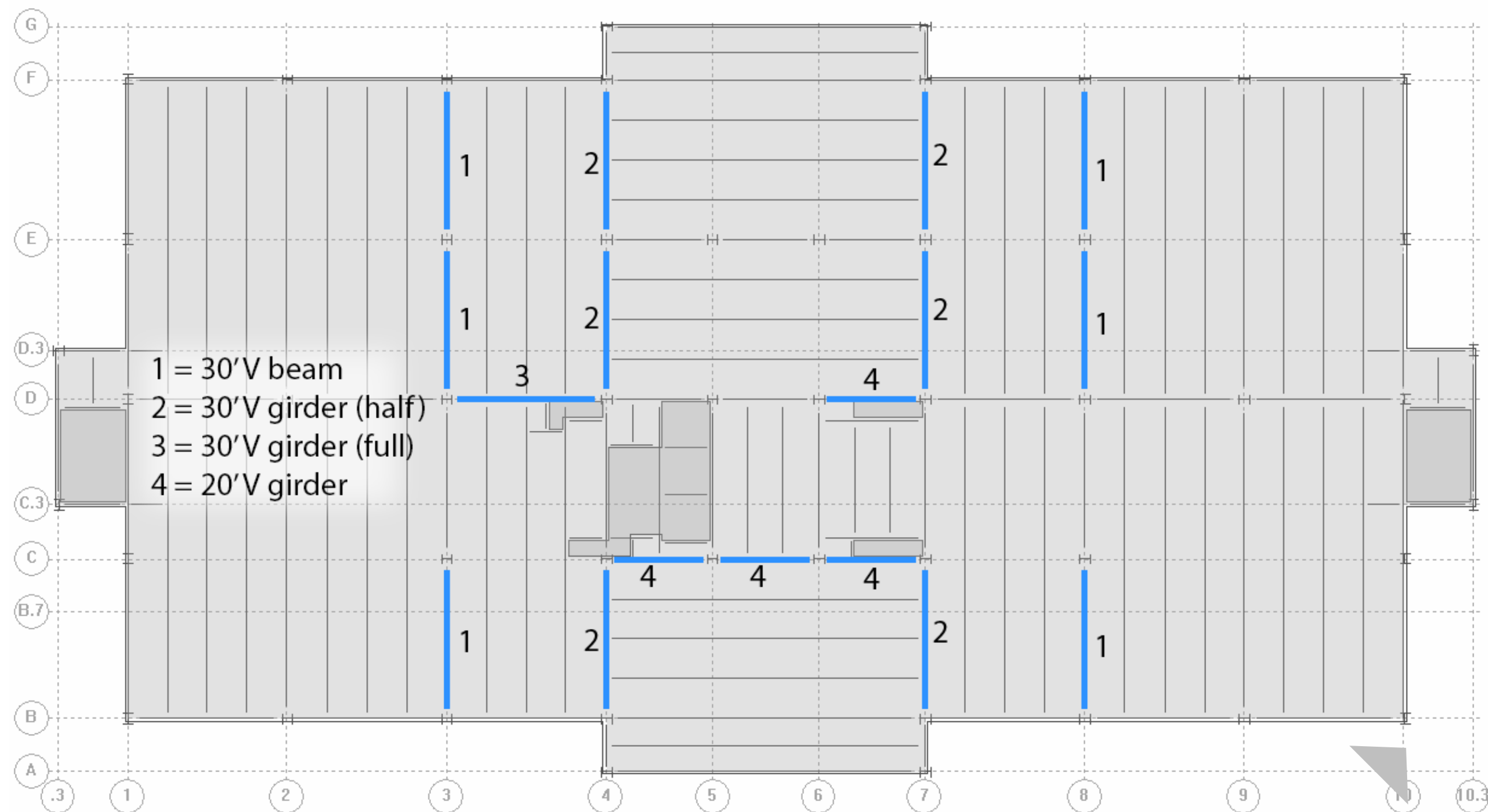


introduction  
proposal  
redesign  
mechanical  
architectural  
conclusion

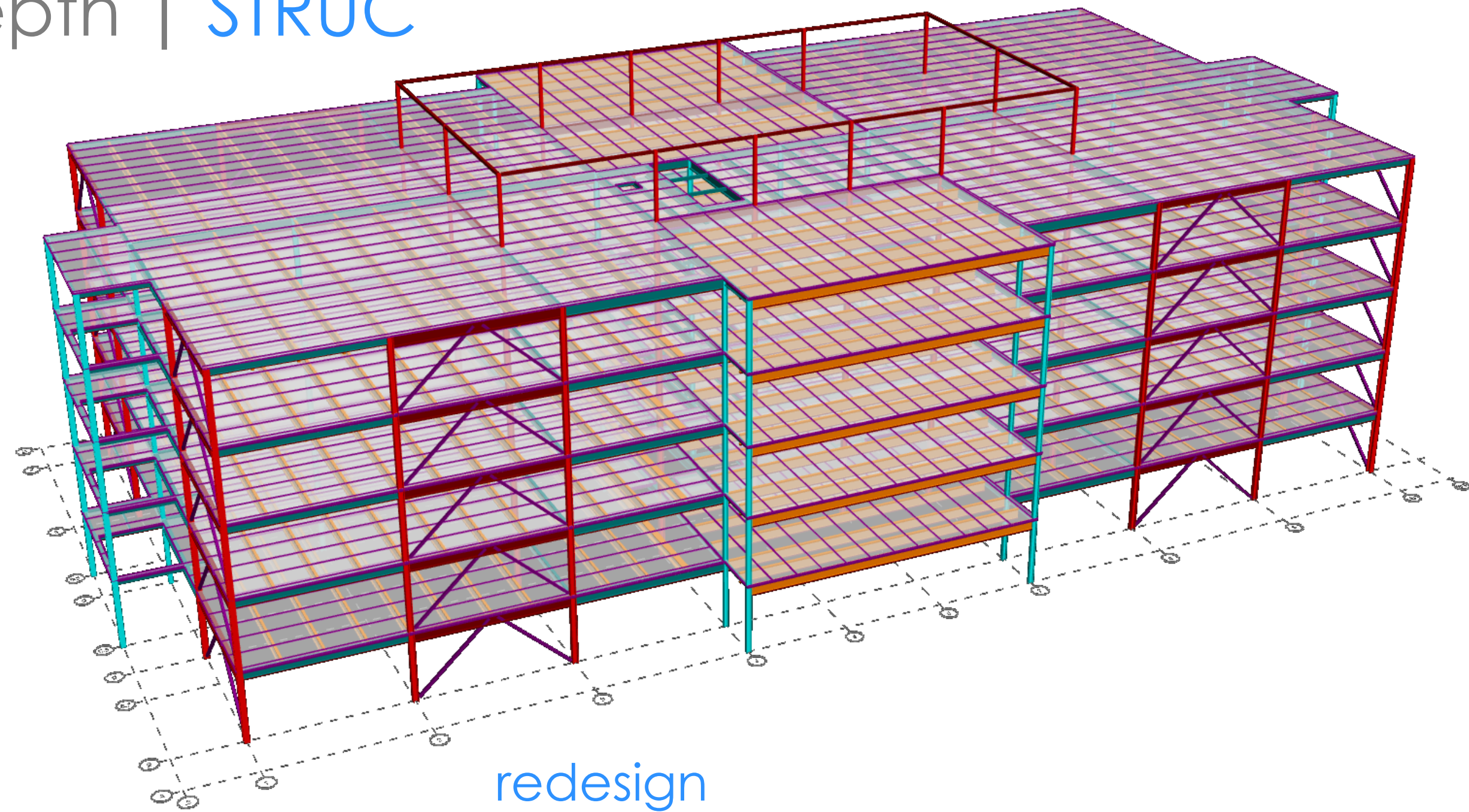
# depth | STRUC vierendeel trusses



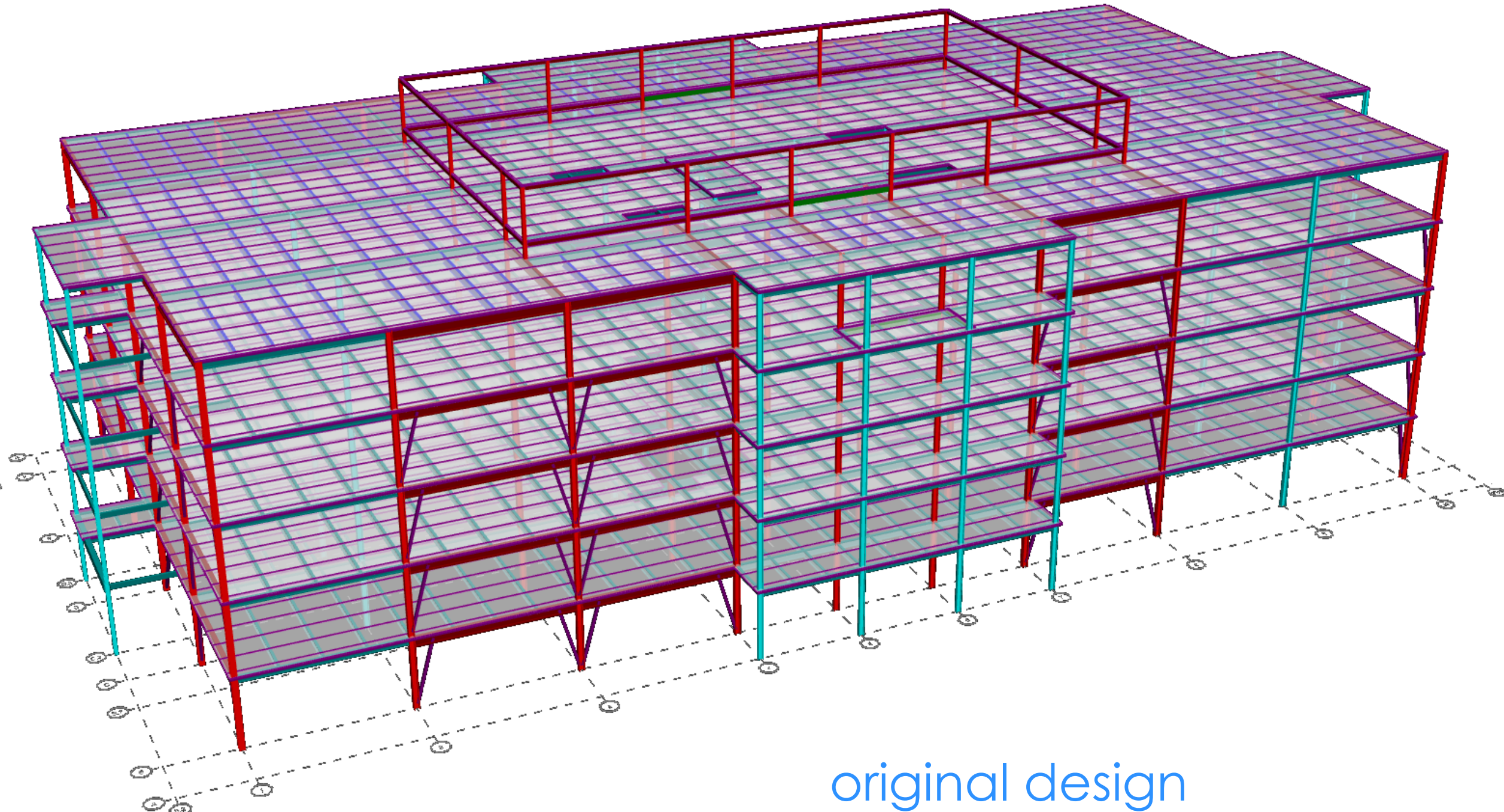
Vierendeel Truss Designs					
Description	Span ft	# panels	Depth in	Size (each member)	quantity
"1" Beam	30	8	27	W8x10	6
"2" Girder (half load)	30	8	27	W8x18	6
"3" Girder (full load)	30	8	27	W8x31	1
"4" Girder	20	6	27	W8x10	4



introduction  
 proposal  
 redesign  
 mechanical  
 architectural  
 conclusion



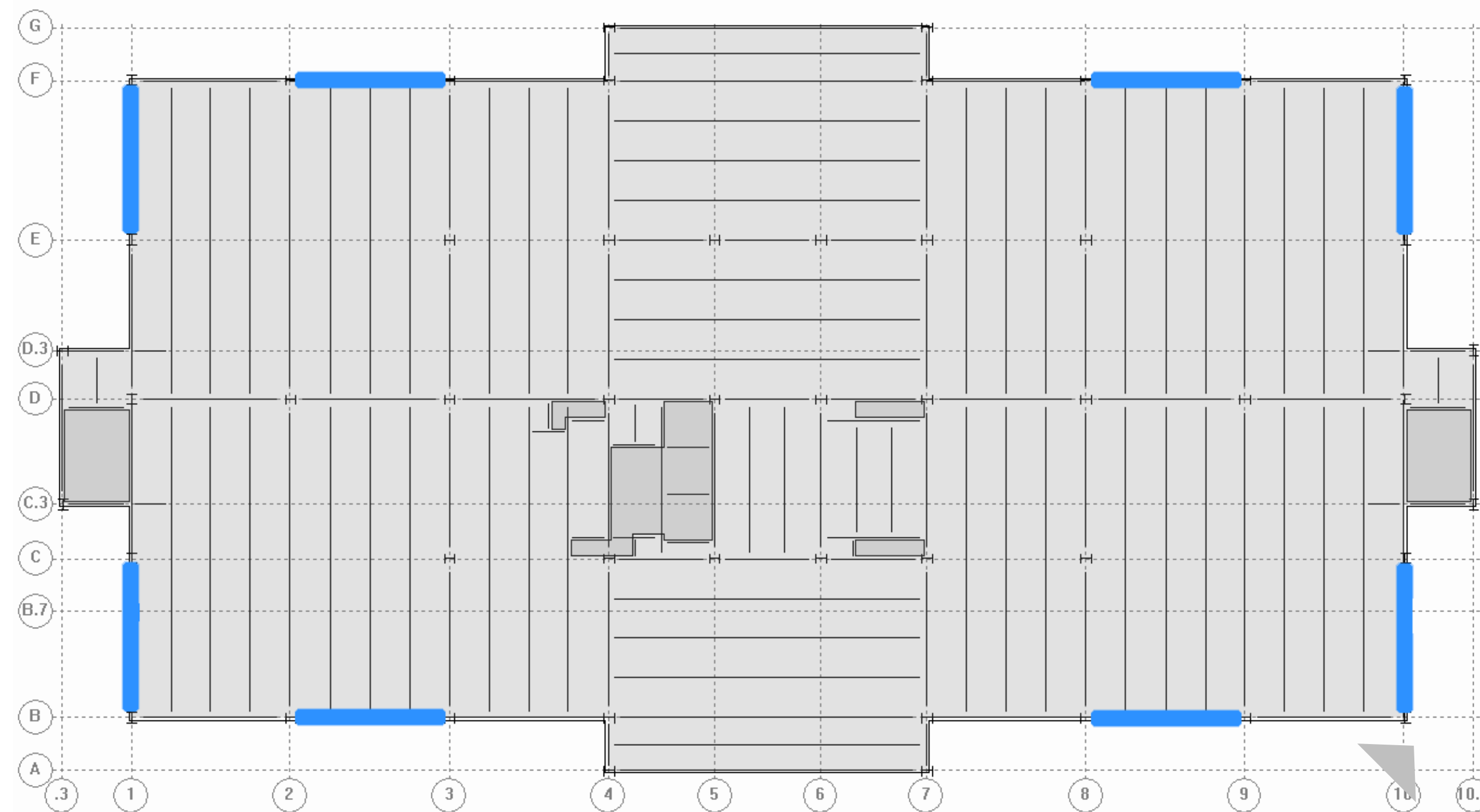
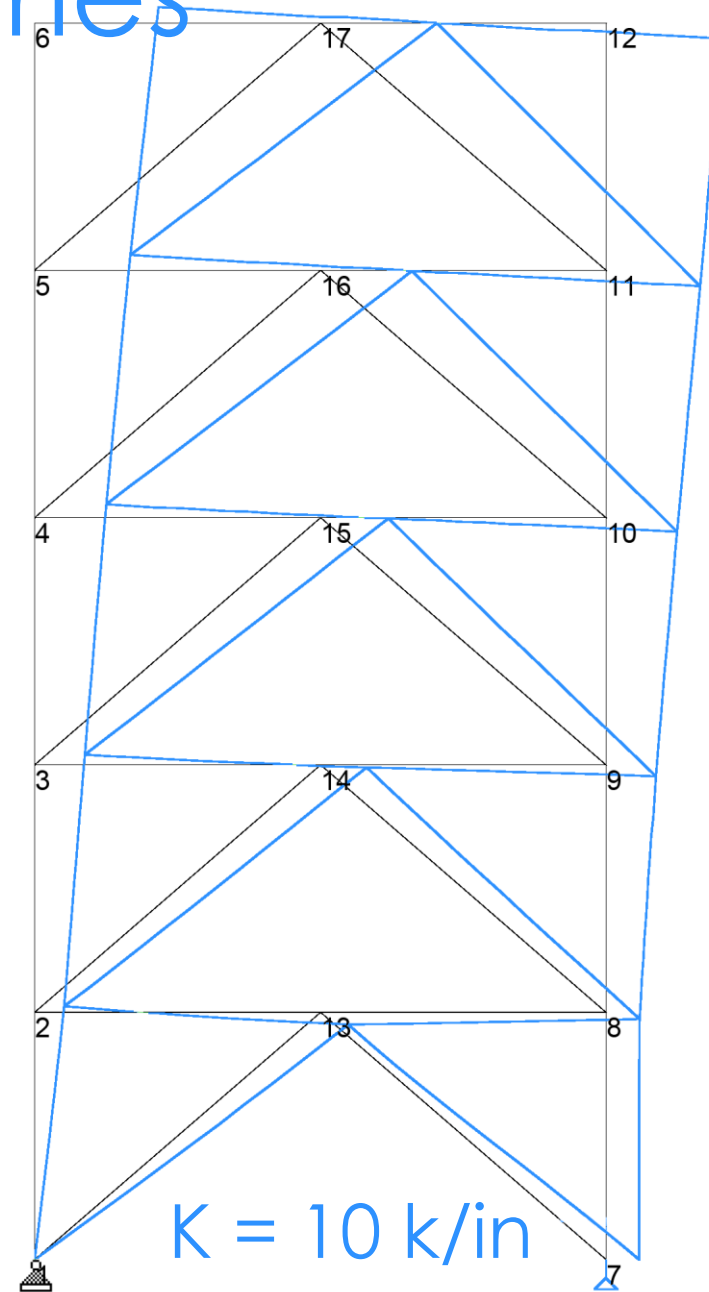
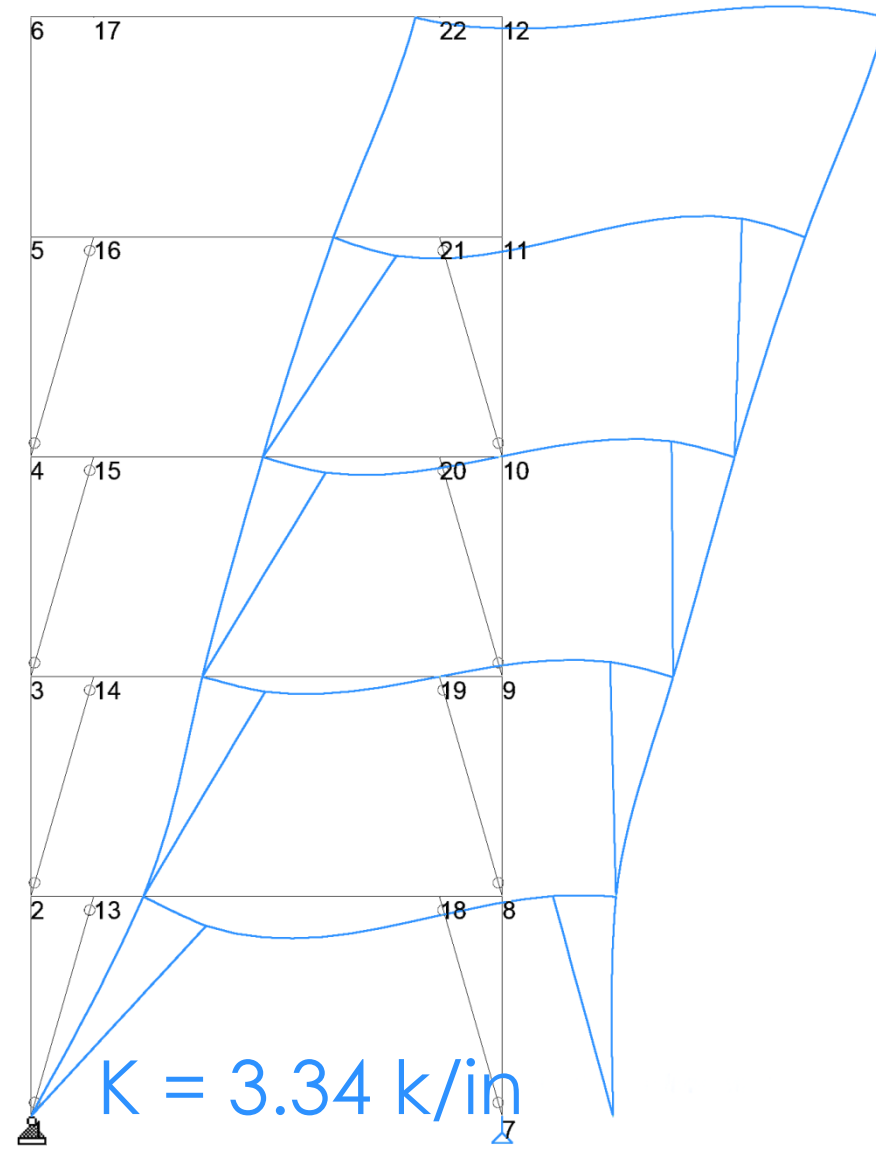
redesign



original design

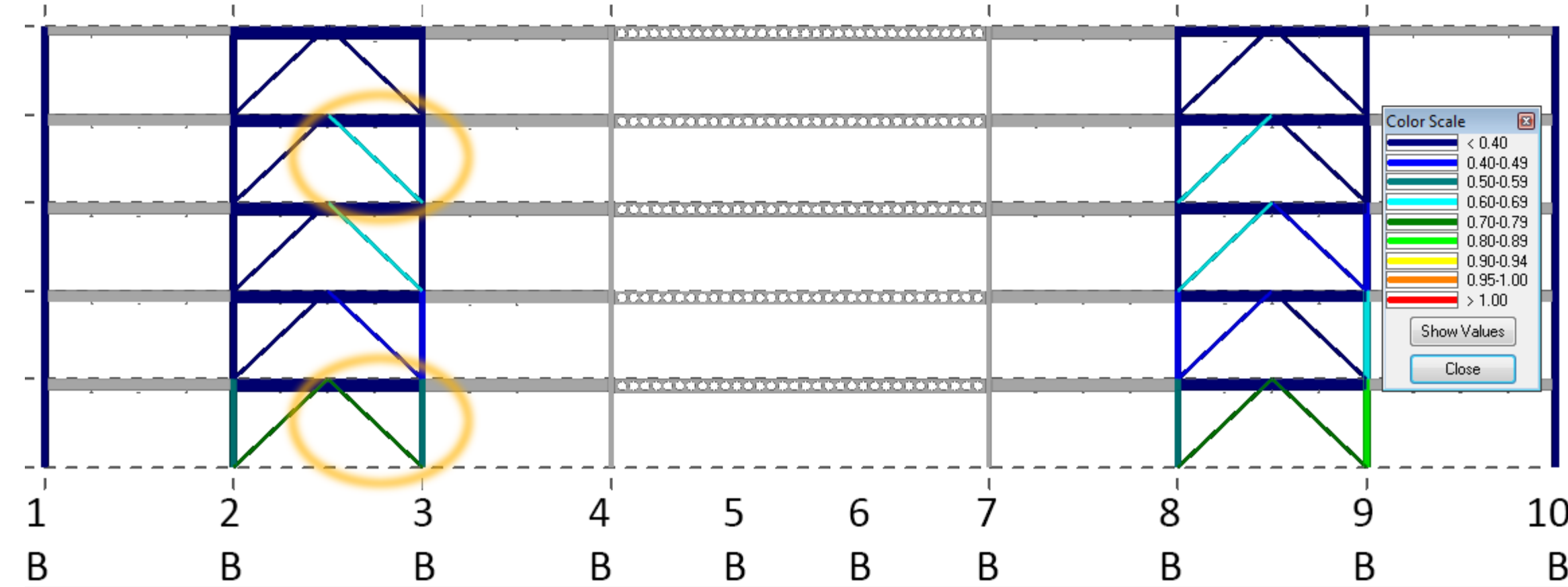
introduction  
proposal  
redesign  
mechanical  
architectural  
conclusion

# depth | STRUC braced frames



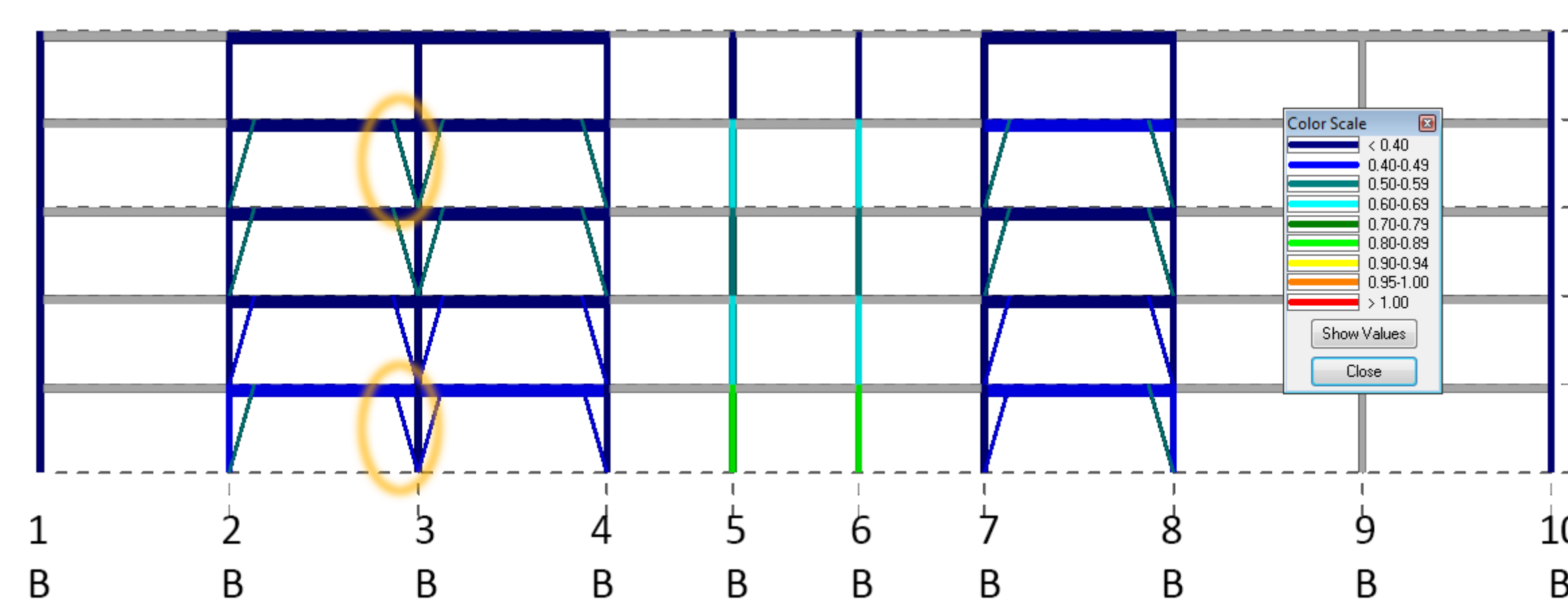
introduction  
proposal  
redesign  
mechanical  
architectural  
conclusion

# depth | STRUC efficiencies



redesign

≈15% more efficient



original design

model	floor	size	max axial (k)	efficiency
original	4 <sup>th</sup> floor	HSS6x6x3/8	71.69	.484
	1 <sup>st</sup> floor	HSS6x6x1/2	85.91	.509
redesign	4 <sup>th</sup> floor	HSS6x6x3/8	62.58	.626
	1 <sup>st</sup> floor	HSS6x6x1/2	84.36	.768

introduction  
proposal  
redesign  
mechanical  
architectural  
conclusion



+ verified cellular beam sizes

+ stiffer concentrically braced frames

+ more efficient lateral system

introduction  
proposal  
redesign  
mechanical  
architectural  
conclusion



introduction  
proposal  
redesign  
mechanical  
architectural  
conclusion

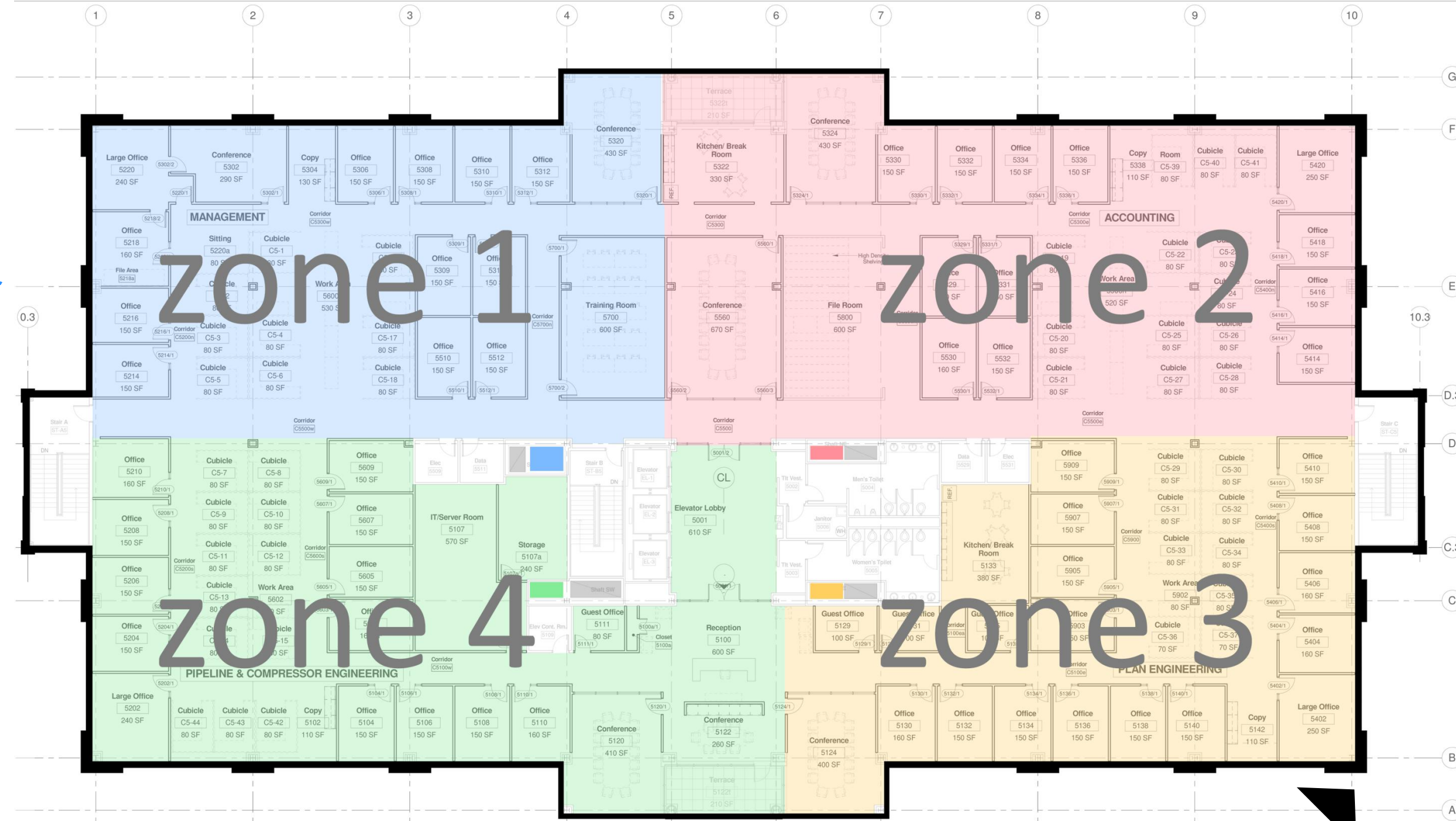


TRACE model – 15,520 CFM/floor



Excel – 14,800 CFM/floor

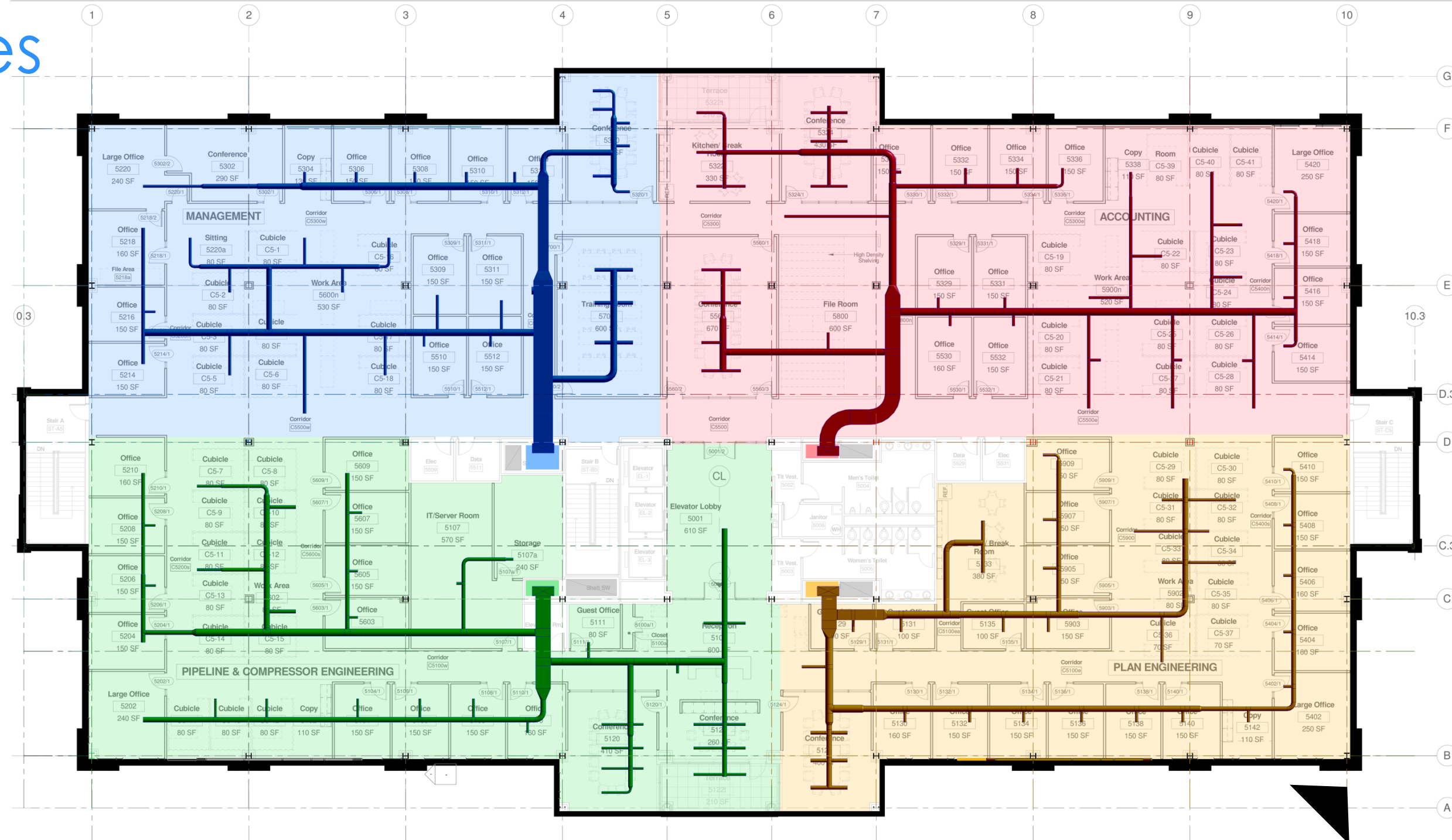
≈ 5% accuracy



introduction  
 proposal  
 redesign  
 mechanical  
 architectural  
 conclusion



# breadth | MECH rtu zones



introduction  
proposal  
redesign  
mechanical  
architectural  
conclusion

# breadth | MECH vav zones

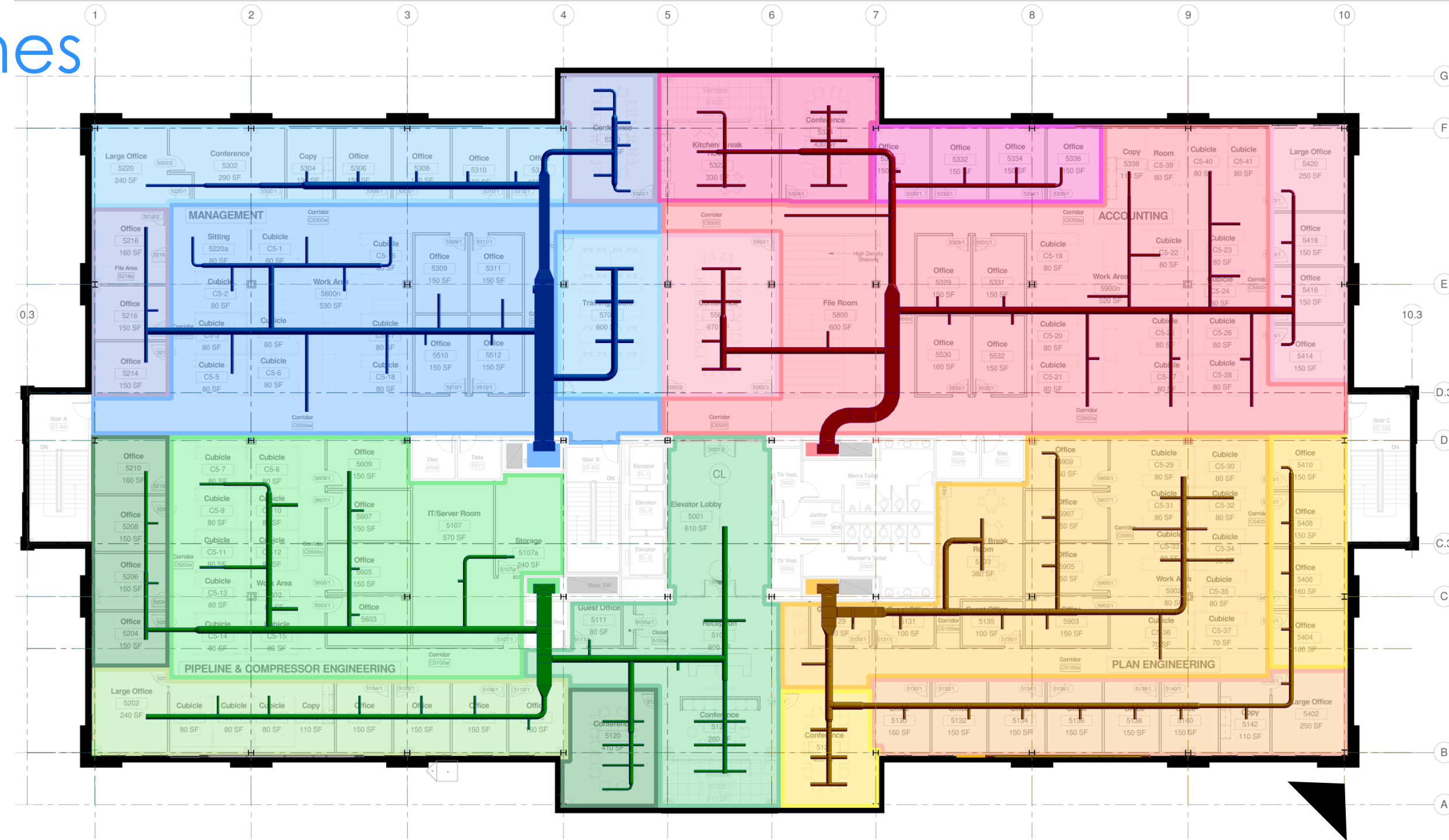


original – 2 Fan Powered Boxes



redesign – 19 VAV boxes

- + edge offices
- + conference spaces
- + interior offices



introduction  
proposal  
redesign  
mechanical  
architectural  
conclusion



+ met IBC height restrictions

+ able to lay out ductwork through structure

+ added VAV boxes for occupant comfort

introduction  
proposal  
redesign  
mechanical  
architectural  
conclusion



55

15

30

introduction  
proposal  
redesign  
mechanical  
architectural  
conclusion

# breadth | ARCH façade



introduction  
proposal  
redesign  
mechanical  
architectural  
conclusion

# breadth | ARCH façade

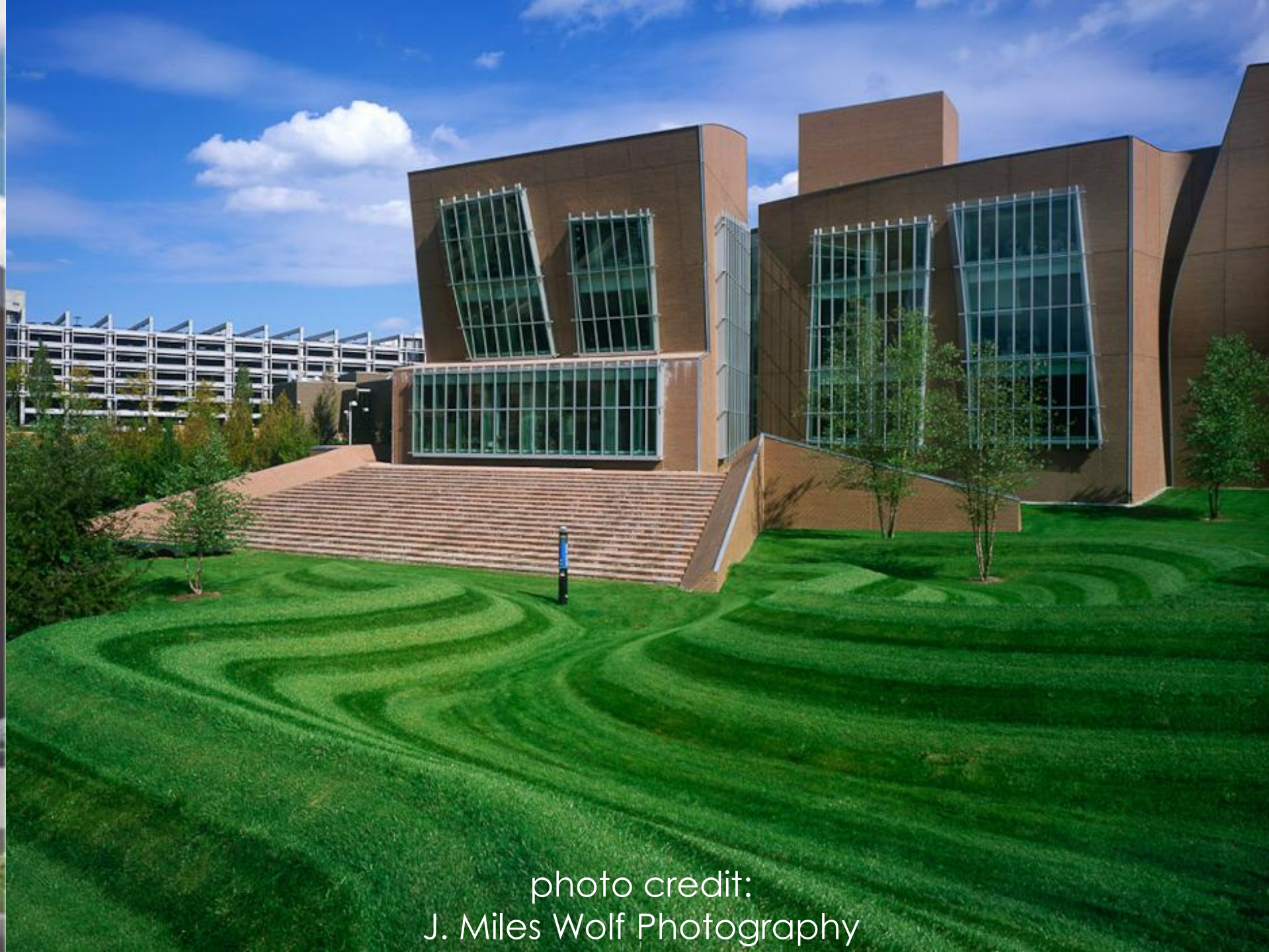


photo credit:  
J. Miles Wolf Photography

inspiration: The Vontz Center,  
Cincinnati

architect: Frank Gehry

introduction  
proposal  
redesign  
mechanical  
architectural  
conclusion

breadth | ARCH façade



inspiration: The Vontz Center,  
Cincinnati

architect: Frank Gehry

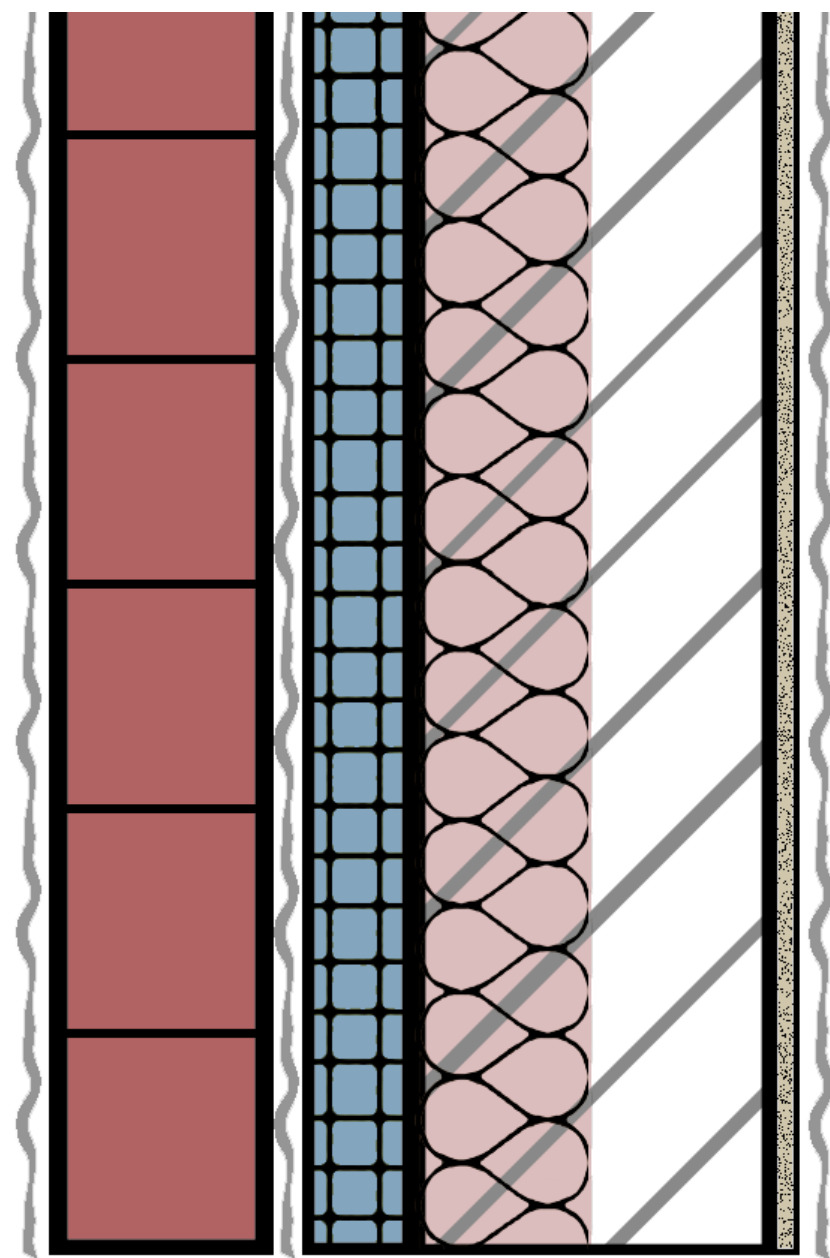
introduction  
proposal  
redesign  
mechanical  
architectural  
conclusion

# breadth | ARCH envelope



original

R = 15.3



schematic section:

- ext air film
- brick
- air gap
- rigid ins
- batt ins/metal studs
- gypsum bd
- int air film

introduction  
proposal  
redesign  
mechanical  
architectural  
conclusion

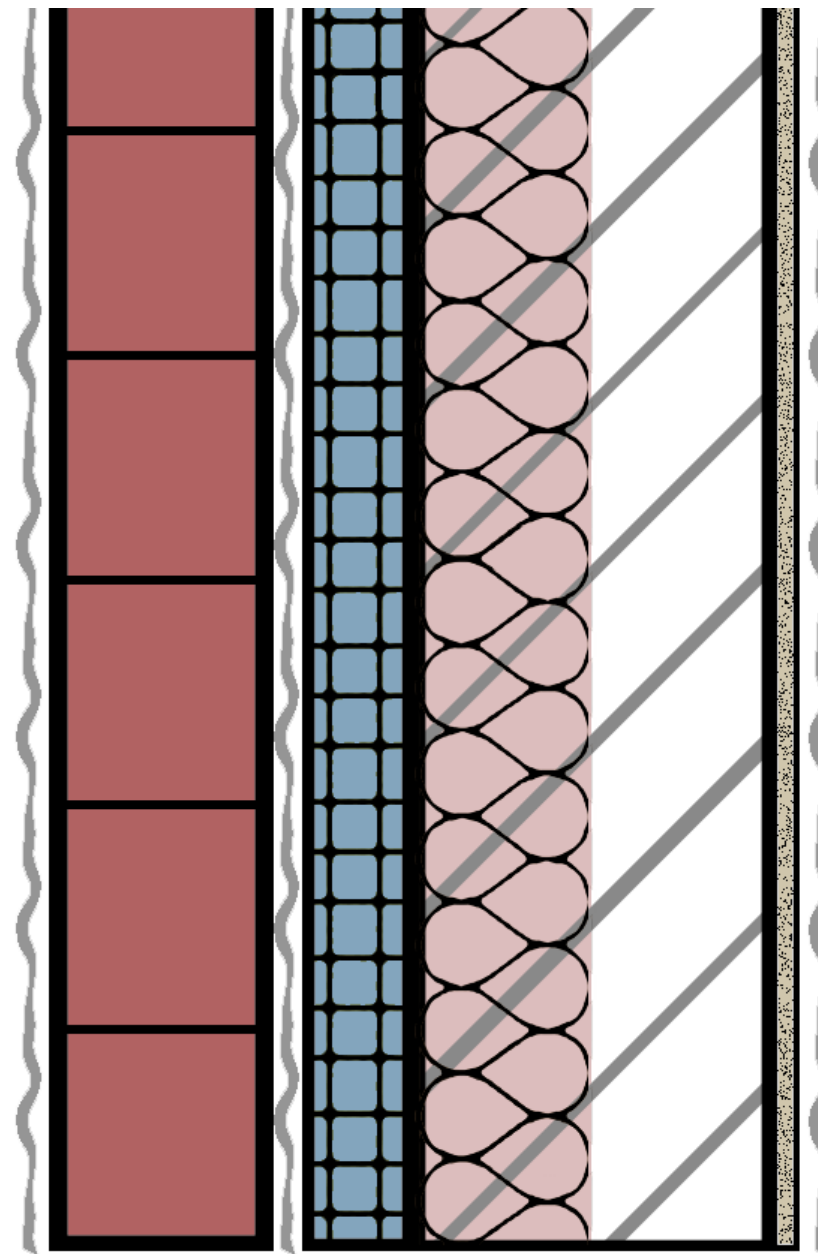


# breadth | ARCH envelope



original

R = 15.3



schematic section:

ext air film  
brick  
air gap  
rigid ins  
batt ins/metal studs  
gypsum bd  
int air film

rigid insulation replacement:

→ [MetalWrap Series](#) (by CENTRIA)

2" rigid insulation

36" x 20' max panel

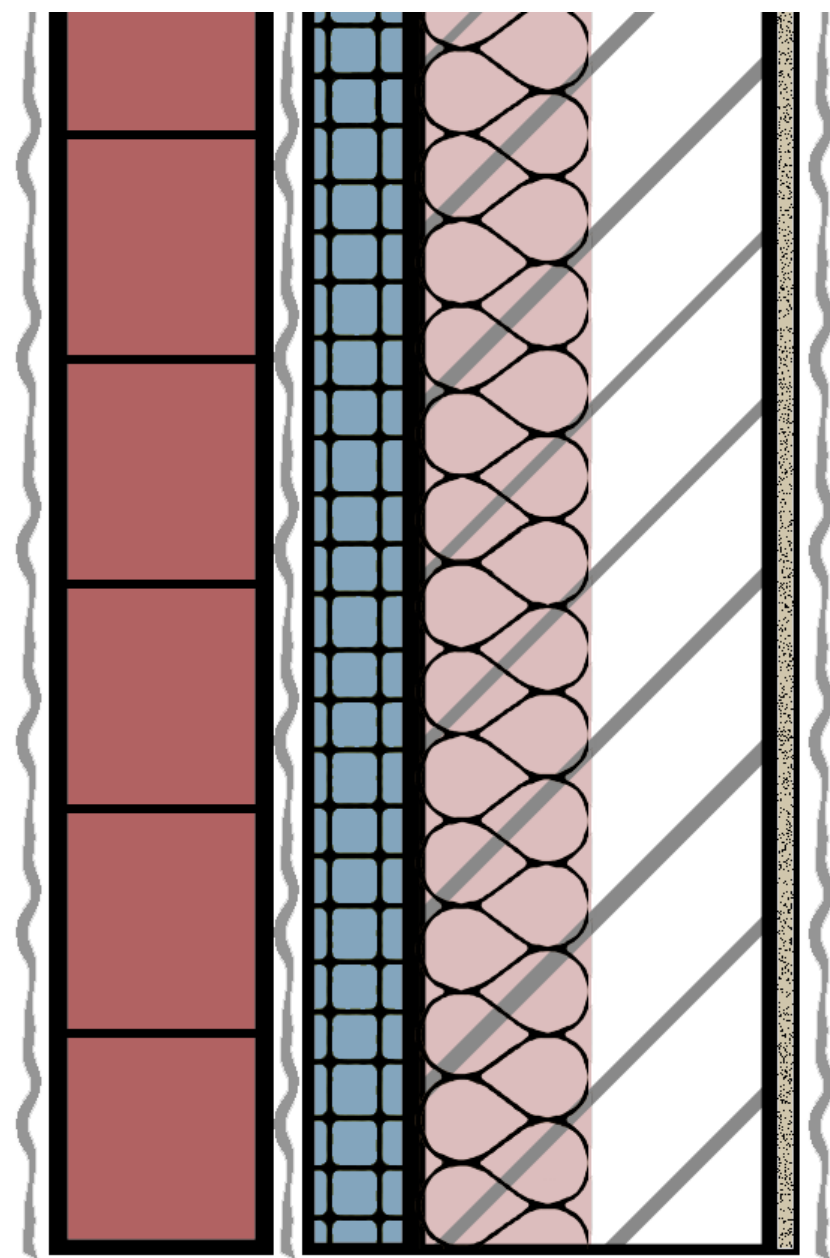
introduction  
proposal  
redesign  
mechanical  
architectural  
conclusion

breadth | ARCH envelope



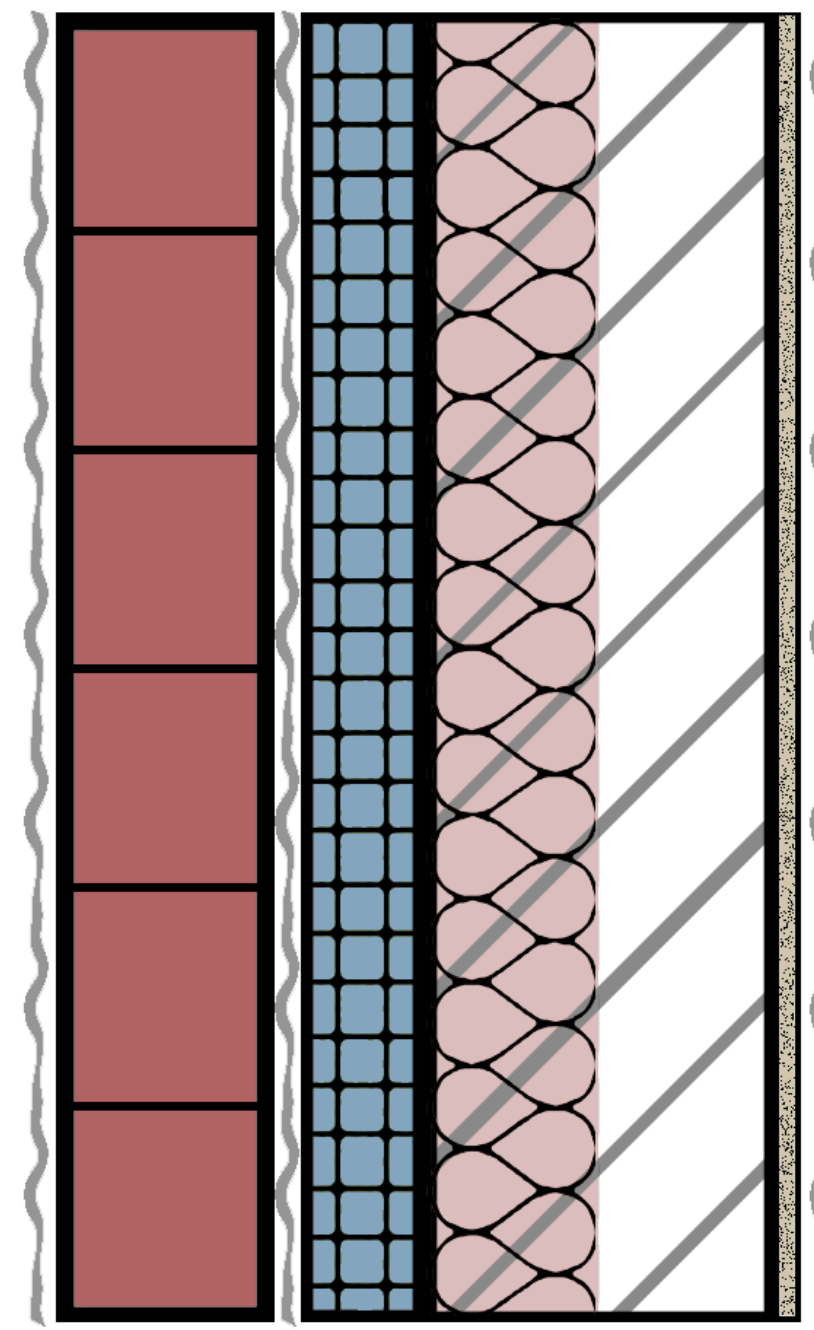
original

$R = 15.3$



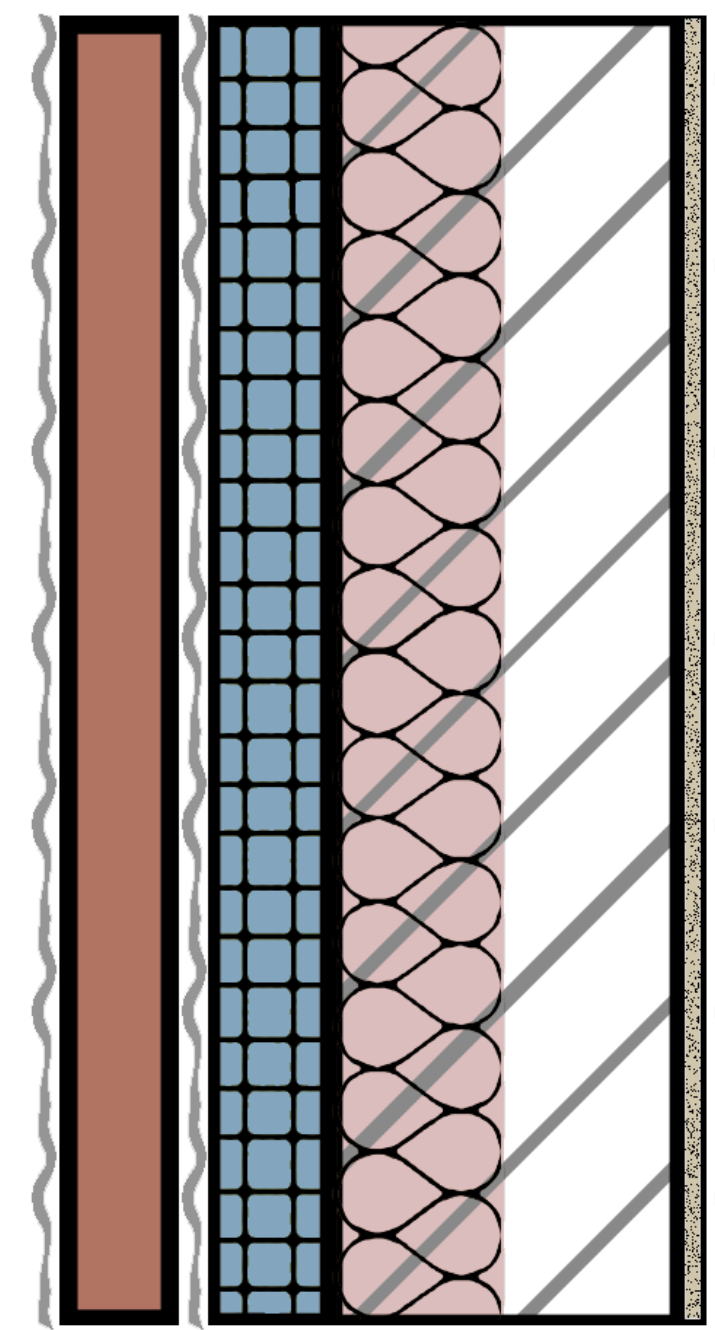
redesigned brick

$R = 22.0$   
44% increase



redesigned metal

$R = 21.6$   
41% increase



introduction  
proposal  
redesign  
mechanical  
architectural  
conclusion



+ redesigned façade with modern materials

+ improved thermal properties of envelope

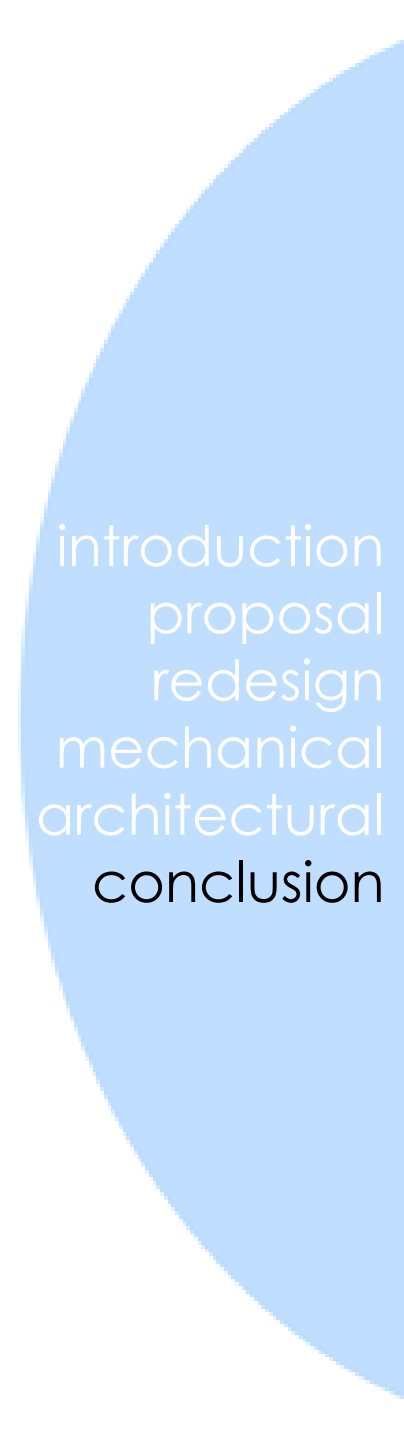
introduction  
proposal  
redesign  
mechanical  
**architectural**  
conclusion

# scenario

tenant looking for more **contemporary** high-end space:

**open** feel

**modern** materials



introduction  
proposal  
redesign  
mechanical  
architectural  
conclusion

# scenario

# conclusion



tenant looking for more **contemporary** high-end space:

**open** feel

**modern** materials

→ **struc** – cellular beams in exposed ceiling  
cellular beams are appropriate to address open feel

concentrically braced frames are more efficient than previous design

introduction  
proposal  
redesign  
mechanical  
architectural  
conclusion

# scenario

# conclusion



tenant looking for more **contemporary** high-end space:

**open** feel

**modern** materials

**struc** – cellular beams in exposed ceiling

cellular beams are appropriate to address open feel

centrically braced frames are more efficient than previous design

**mech** – run through structure (IBC height restriction)

in accommodating the height restriction set by the IBC, the mechanical ductwork is able to be completely laid out within the structural cells

introduction  
proposal  
redesign  
mechanical  
architectural  
conclusion

# scenario

# conclusion

tenant looking for more **contemporary** high-end space:

**open** feel

**modern** materials

**struc** – cellular beams in exposed ceiling

cellular beams are appropriate to address open feel

centrically braced frames are more efficient than previous design

**arch** – façade redesign (aesthetics + thermal)

the façade redesign showcased the braced frames to reflect the contemporary style of the building

thermal properties were improved by switching to a higher-end rigid insulation panel envelope system

**mech** – run through structure (IBC height restriction)

in accommodating the height restriction set by the IBC, the mechanical ductwork is able to be completely laid out within the structural cells

introduction  
proposal  
redesign  
mechanical  
architectural  
conclusion



# acknowledgements

## Atlantic Engineering Services

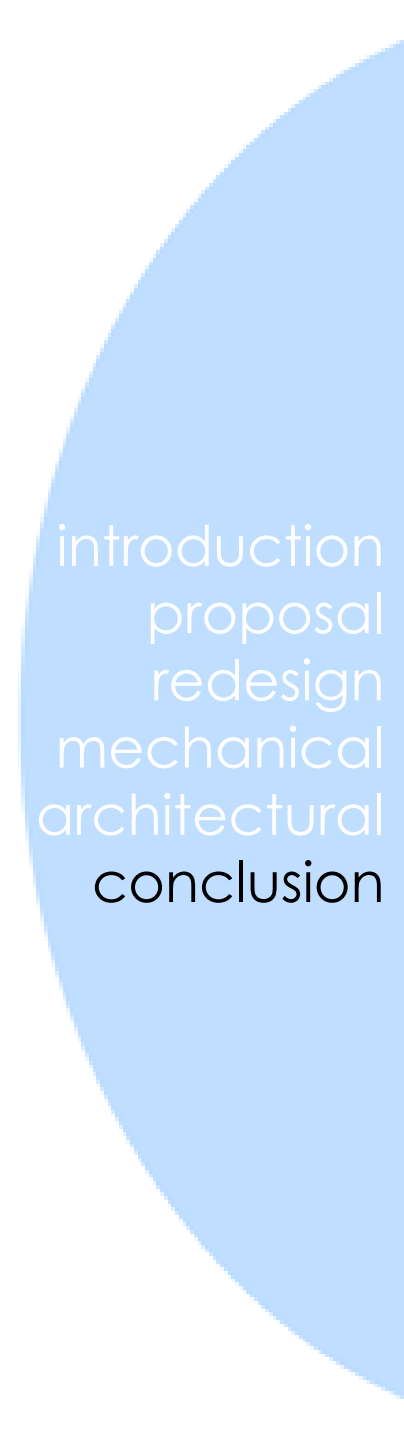

John Schneider  
Angelo Maione  
Justin Kovach

## entire ae faculty

Dr. Thomas Boothby  
Professor M. Kevin Parfitt  
Professor Robert Holland

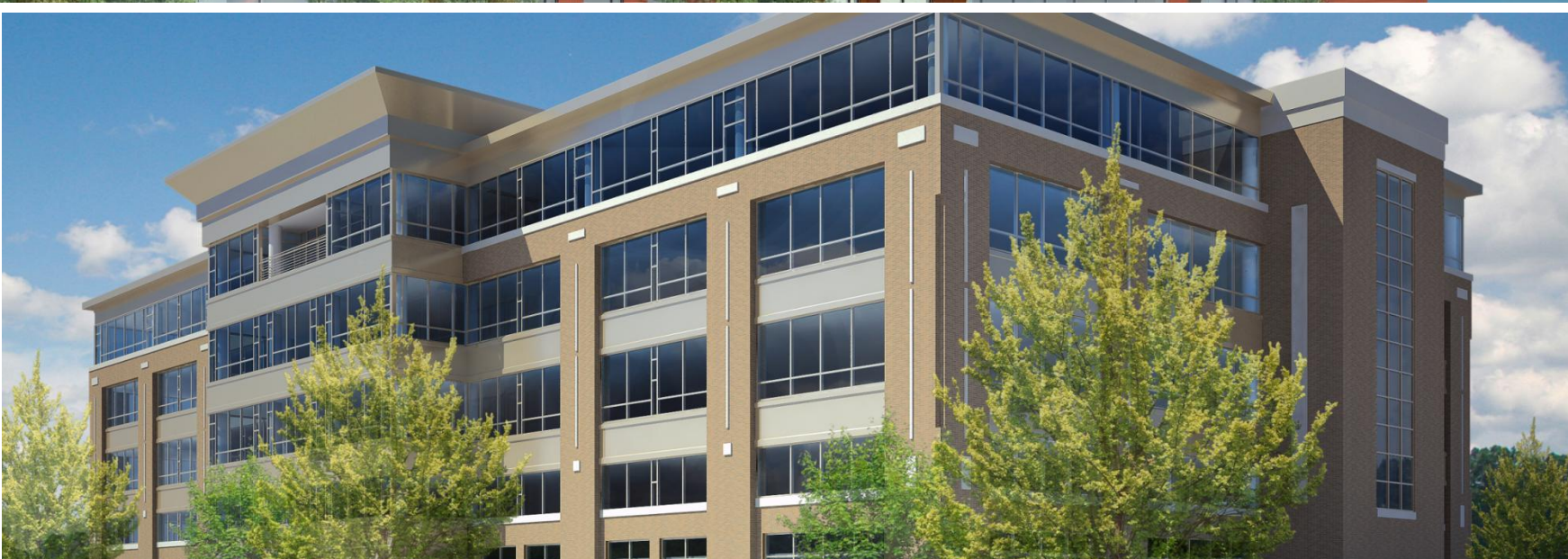
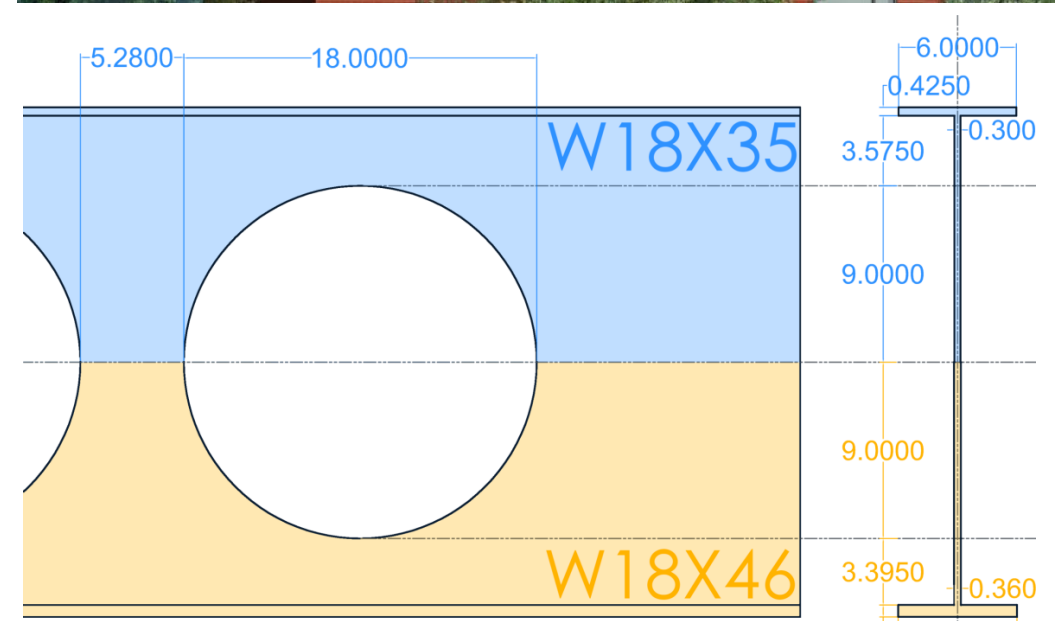
fellow ae students

family + friends



introduction  
proposal  
redesign  
mechanical  
architectural  
conclusion



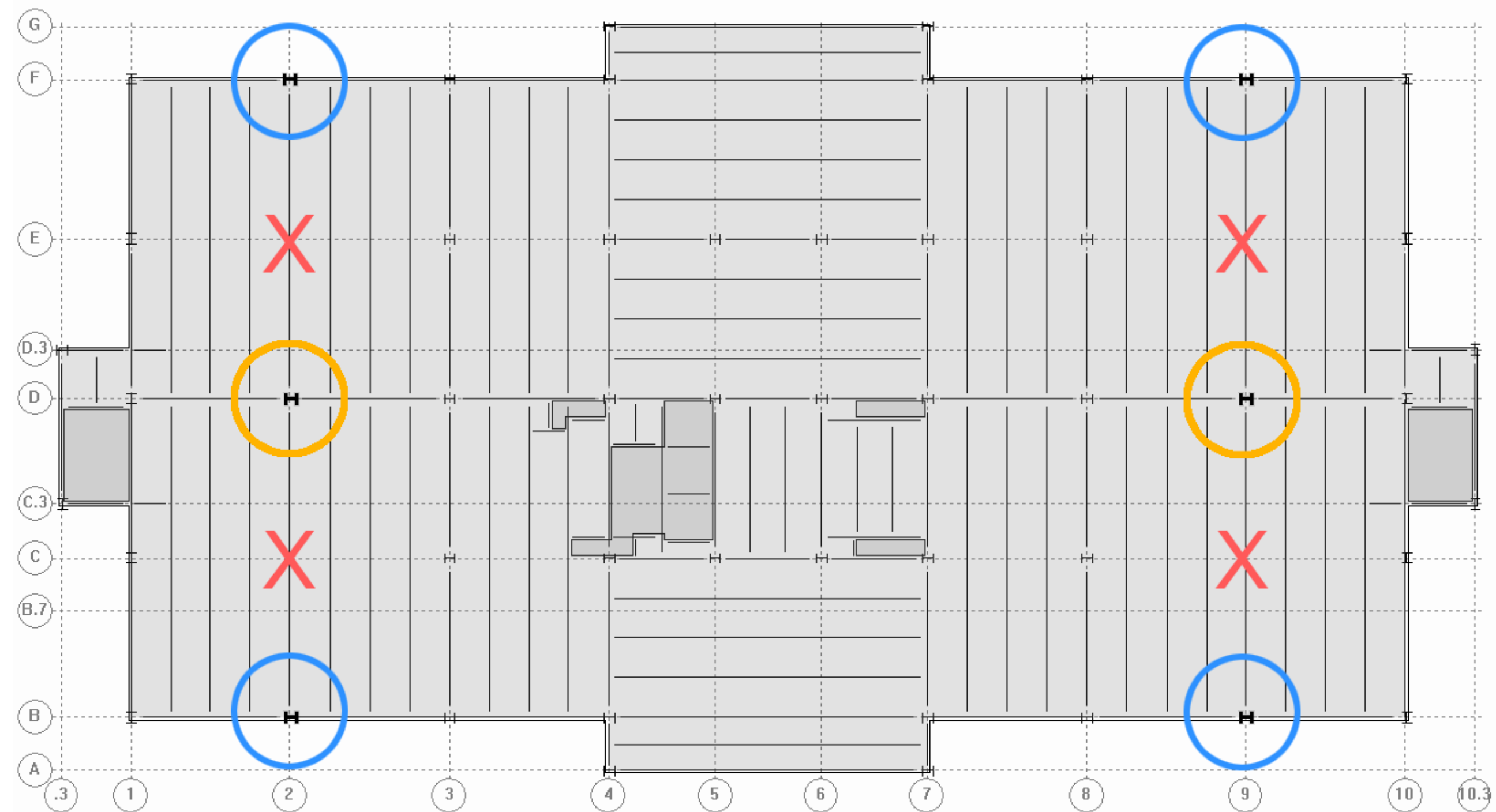


introduction  
proposal  
redesign  
mechanical  
architectural  
conclusion

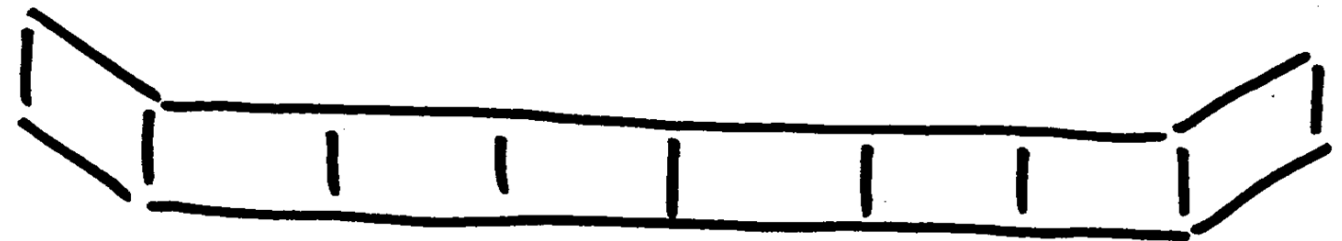
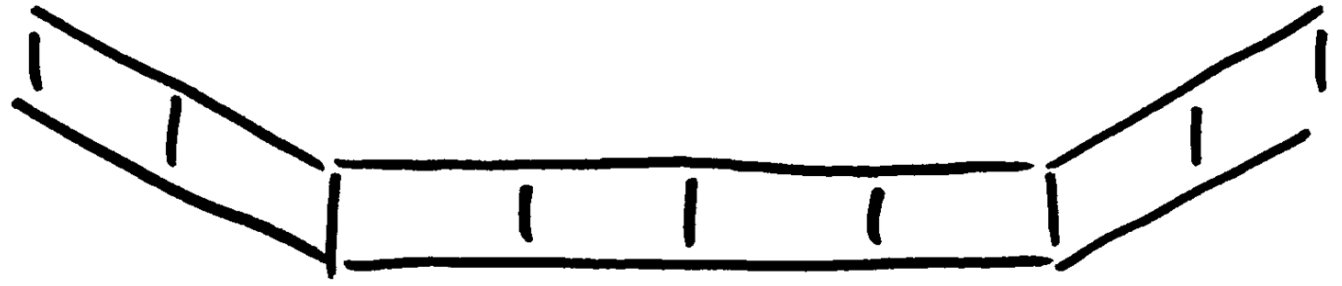
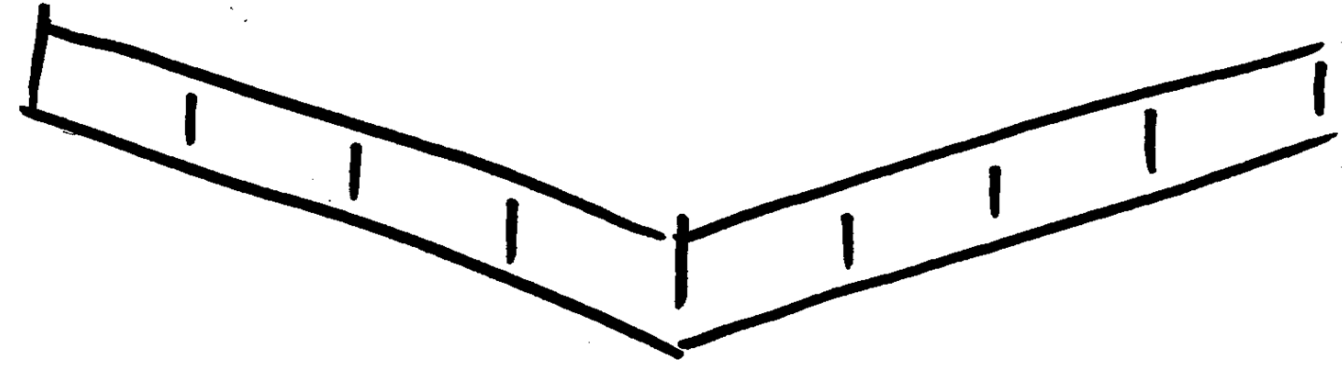


30% increase in foundation load

60% increase in foundation load



depth | STRUC plastic analysis – upper bound theorem



$$\delta W_{int} = \delta W_{ext}$$

$$\sum P \cdot d_i \cdot \theta = \sum M_{p,i} \cdot \theta$$

# IBC 2009 height requirements

Table 503

Type II A  
B (business)

5 stories max ≤ 5 stories (good)  
37,500 SF max ≥ 28,800 SF (good)  
65' max < 70'  
(must reduce to 65' height)

Table 601

Type II A  
Primary Structure

→ 1 hour fire rating

note d: 1 hour fire rating substituted by sprinkler  
(exposed ceiling OK)

## SECTION 503 GENERAL BUILDING HEIGHT AND AREA LIMITATIONS

TABLE 503  
ALLOWABLE BUILDING HEIGHTS AND AREAS<sup>a</sup>  
Building height limitations shown in feet above grade plane. Story limitations shown as stories above grade plane.  
Building area limitations shown in square feet, as determined by the definition of "Area, building," per story

GROUP		TYPE OF CONSTRUCTION							
		TYPE I		TYPE II		TYPE III		TYPE IV	T
		A	B	A	B	A	B	HT	A
		UL	160	65	55	65	55	65	50
		STORIES(S) AREA (A)							
A-1	S A	UL UL	5 UL	3 15,500	2 8,500	3 14,000	2 8,500	3 15,000	2 11,500
A-2	S A	UL UL	11 UL	3 15,500	2 9,500	3 14,000	2 9,500	3 15,000	2 11,500
A-3	S A	UL UL	11 UL	3 15,500	2 9,500	3 14,000	2 9,500	3 15,000	2 11,500
A-4	S A	UL UL	11 UL	3 15,500	2 9,500	3 14,000	2 9,500	3 15,000	2 11,500
A-5	S A	UL UL	UL UL	UL UL	UL UL	UL UL	UL UL	UL UL	UL UL
B	S A	UL UL	11 UL	5 37,500	3 23,000	5 28,500	3 19,000	5 36,000	3 18,000
E	S A	UL UL	5 UL	3 26,500	2 14,500	3 23,500	2 14,500	3 25,500	1 18,500
F-1	S A	UL UL	11 UL	4 25,000	2 15,500	3 19,000	2 12,000	4 33,500	2 14,000
F-2	S A	UL UL	11 UL	5 37,500	3 23,000	4 28,500	3 18,000	5 50,500	3 21,000
H-1	S A	1 21,000	1 16,500	1 11,000	1 7,000	1 9,500	1 7,000	1 10,500	1 7,500

## TABLE 601 FIRE-RESISTANCE RATING REQUIREMENTS FOR BUILDING ELEMENTS (hours)

BUILDING ELEMENT	TYPE I		TYPE II		TYPE III		TYPE IV	TYPE V	
	A	B	A <sup>d</sup>	B	A <sup>d</sup>	B	HT	A <sup>d</sup>	B
Primary structural frame <sup>g</sup> (see Section 202)	3 <sup>a</sup>	2 <sup>a</sup>	1	0	1	0	HT	1	0
Bearing walls Exterior <sup>f, g</sup> Interior	3 3 <sup>a</sup>	2 2 <sup>a</sup>	1 1	0 0	2 1	2 0	2 1/HT	1 1	0 0
Nonbearing walls and partitions Exterior	See Table 602								
Nonbearing walls and partitions Interior <sup>e</sup>	0	0	0	0	0	0	See Section 602.4.6	0	0
Floor construction and secondary members (see Section 202)	2	2	1	0	1	0	HT	1	0
Roof construction and secondary members (see Section 202)	1 <sup>1/2</sup> <sup>b</sup>	1 <sup>b,c</sup>	1 <sup>b,c</sup>	0 <sup>c</sup>	1 <sup>b,c</sup>	0	HT	1 <sup>b,c</sup>	0

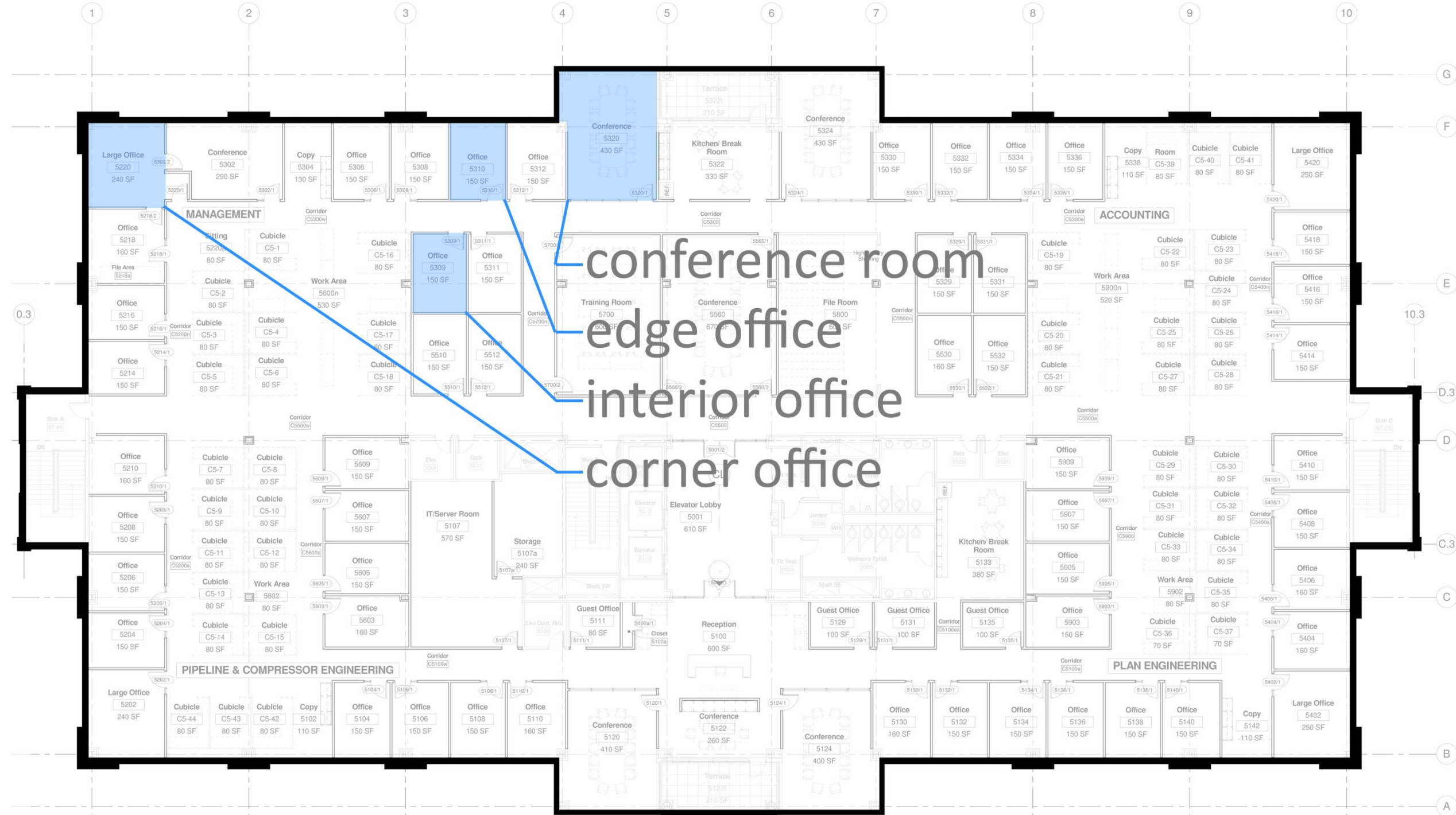
For SI: 1 foot = 304.8 mm.

- a. Roof supports: Fire-resistance ratings of primary structural frame and bearing walls are permitted to be reduced by 1 hour where supporting a roof only.
- b. Except in Group F-1, H, M and S-1 occupancies, fire protection of structural members shall not be required, including protection of roof framing and decking where every part of the roof construction is 20 feet or more above any floor immediately below. Fire-retardant-treated wood members shall be allowed to be used for such unprotected members.
- c. In all occupancies, heavy timber shall be allowed where a 1-hour or less fire-resistance rating is required.
- d. An approved automatic sprinkler system in accordance with Section 903.3.1.1 shall be allowed to be substituted for 1-hour fire-resistance-rated construction, provided such system is not otherwise required by other provisions of the code or used for an allowable area increase in accordance with Section 506.3 or an allowable height increase in accordance with Section 504.2. The 1-hour substitution for the fire resistance of exterior walls shall not be permitted.
- e. Not less than the fire-resistance rating required by other sections of this code.
- f. Not less than the fire-resistance rating based on fire separation distance (see Table 602).
- g. Not less than the fire-resistance rating as referenced in Section 704.10



TRACE 700 - room checksums					excel	
room type	# people	coil airflow (cfm)	capacity (ton) (MBh)		air flow (cfm)	ventilation (cfm)
corner office	1	280	0.5	6.3	75	19.4
edge office	1	125	0.3	3.1	75	14
interior office	1	25	0.2	1.8	75	14
conference room	22	425	1.5	17.4	475	95.8

TRACE 700 - system checksums					excel
AHU	# people	coil airflow (cfm)	capacity (ton) (MBh)		airflow (cfm)
1	85	3250	9.9	118.6	3875
2	82	3450	11.2	134.4	4100
3	43	4100	8.9	106.5	3225
4	60	4720	11.6	139.4	3600
		<b>Σ 15520</b>			<b>Σ 14800</b>



# MetalWrap

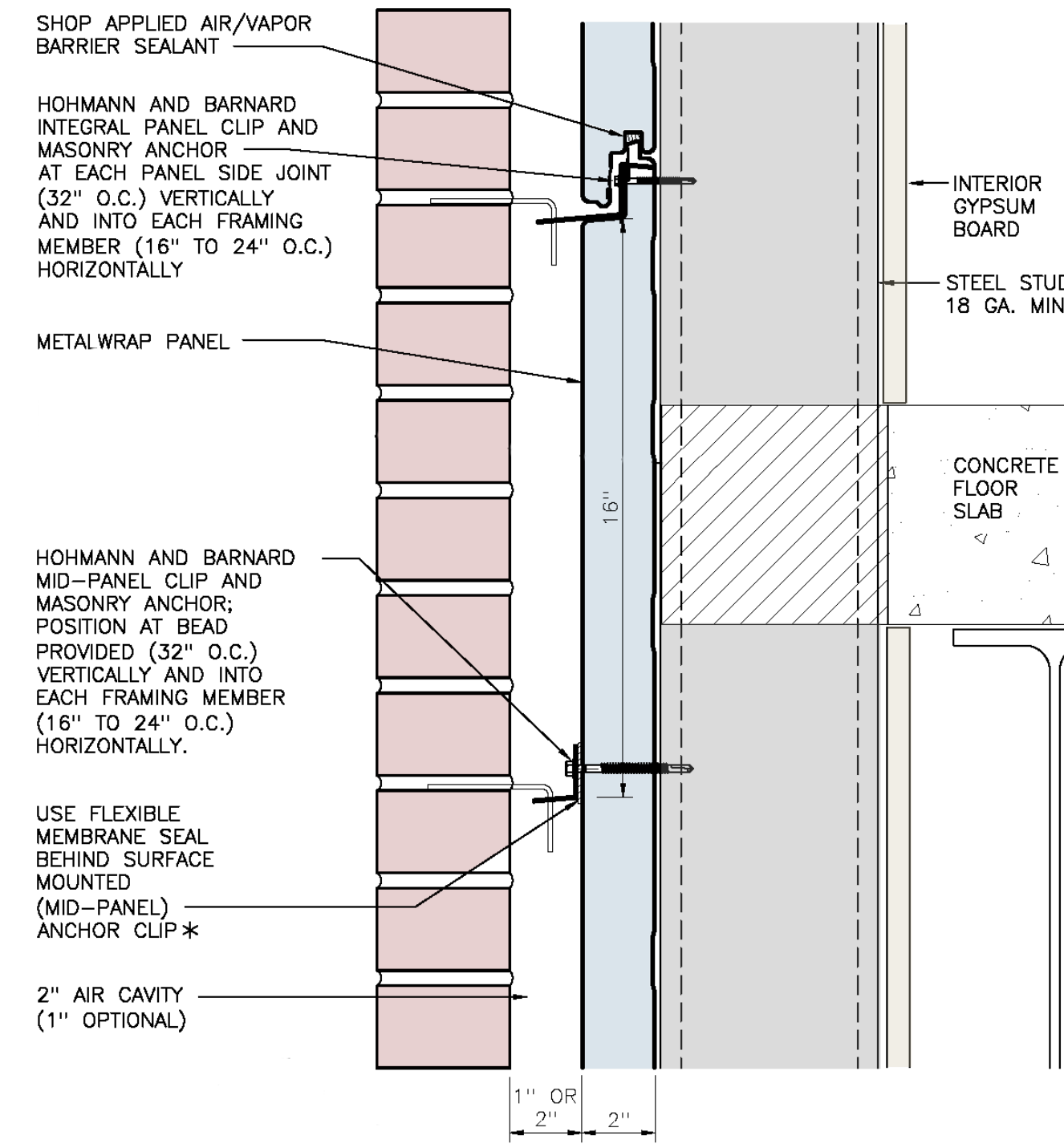
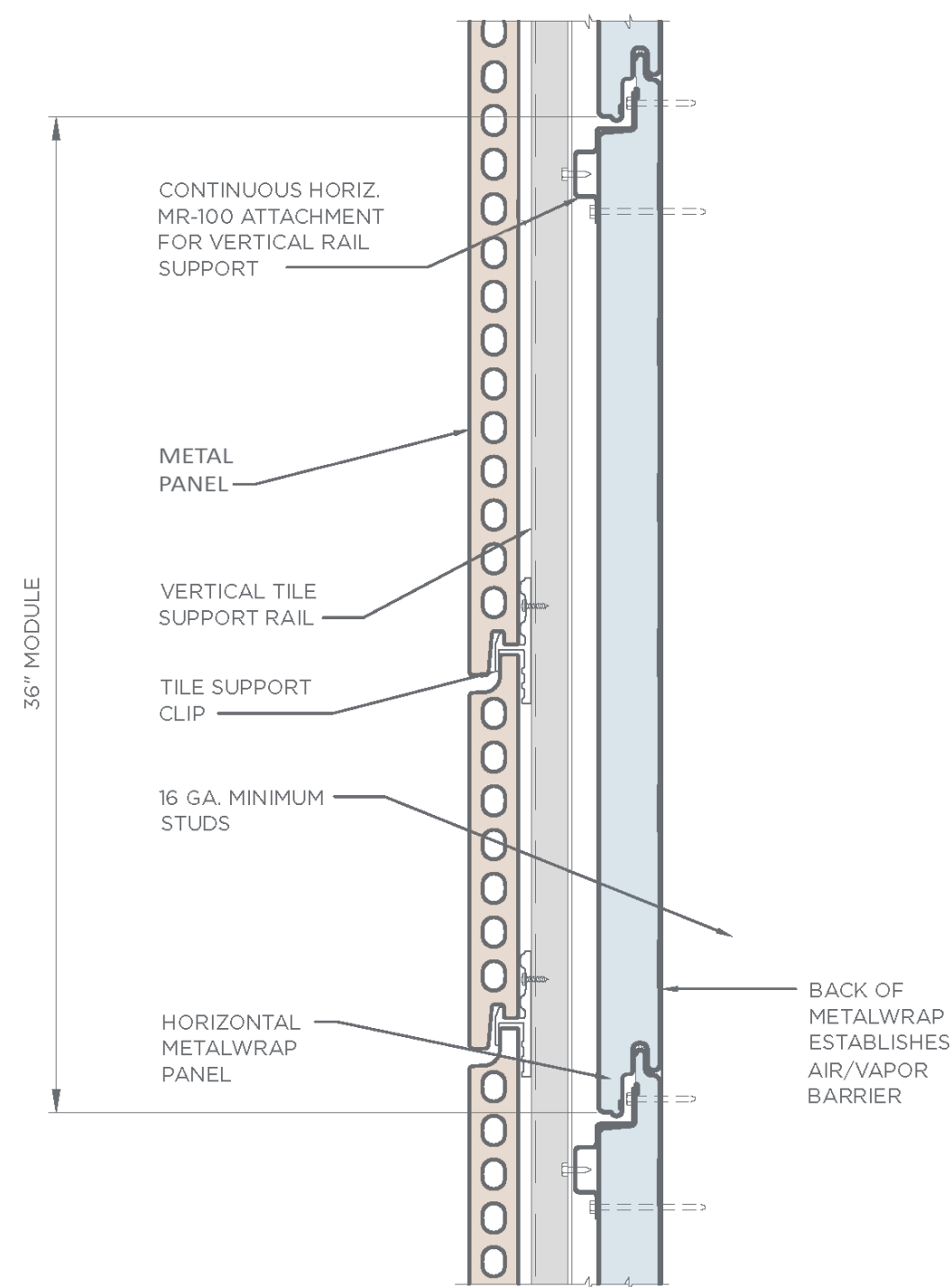
## MetalWrap MR-300 (center)

- 36" x 20' max panel
- 2" rigid insulation
- 2.5" nominal architectural panel thickness



## MetalWrap for Masonry (right)

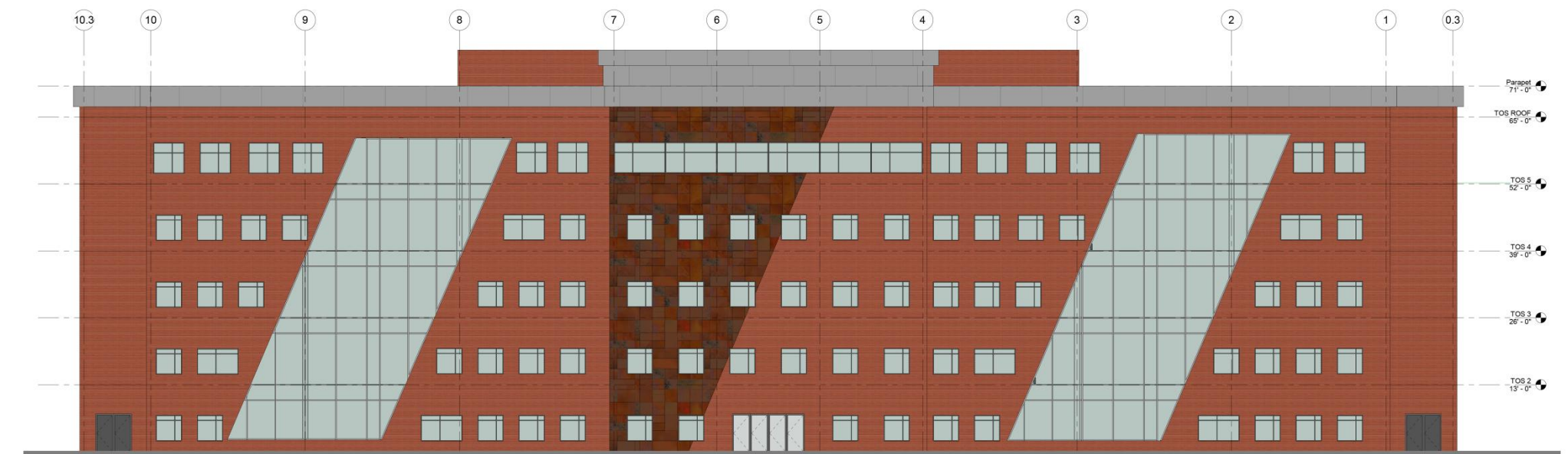
- 2" rigid insulation
- 32" x 20' max panel



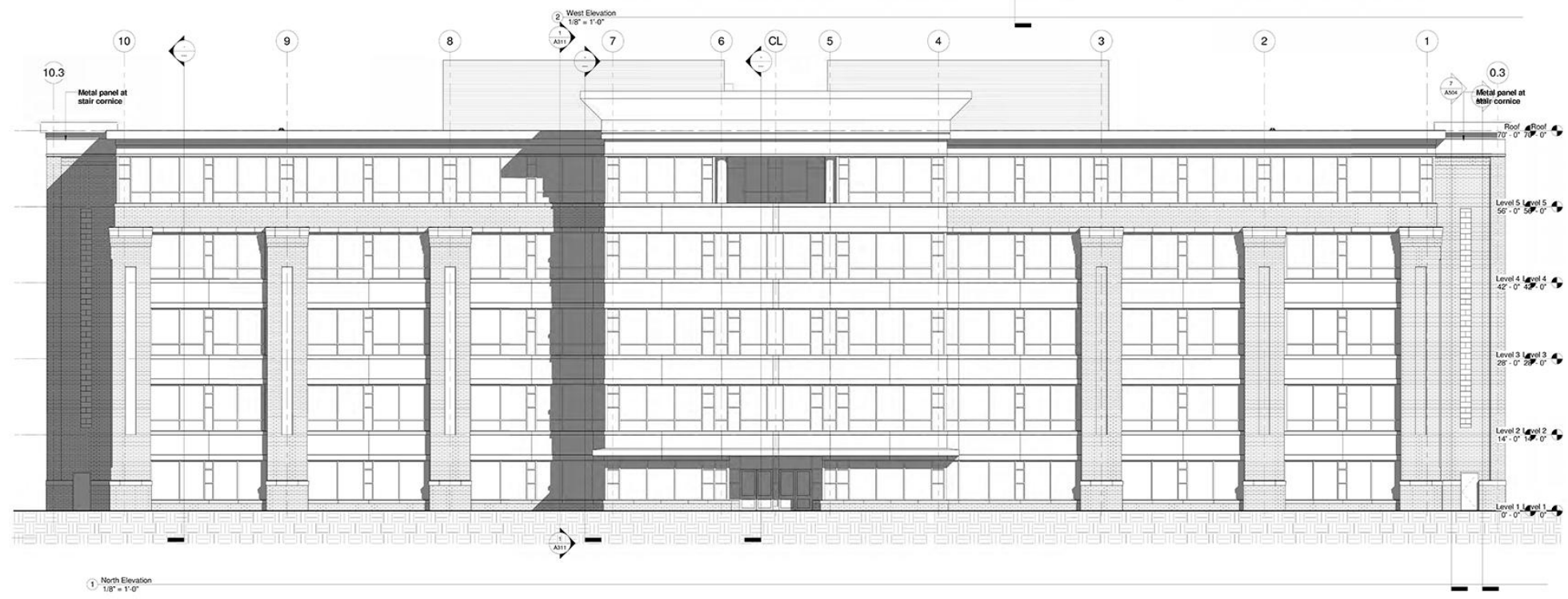
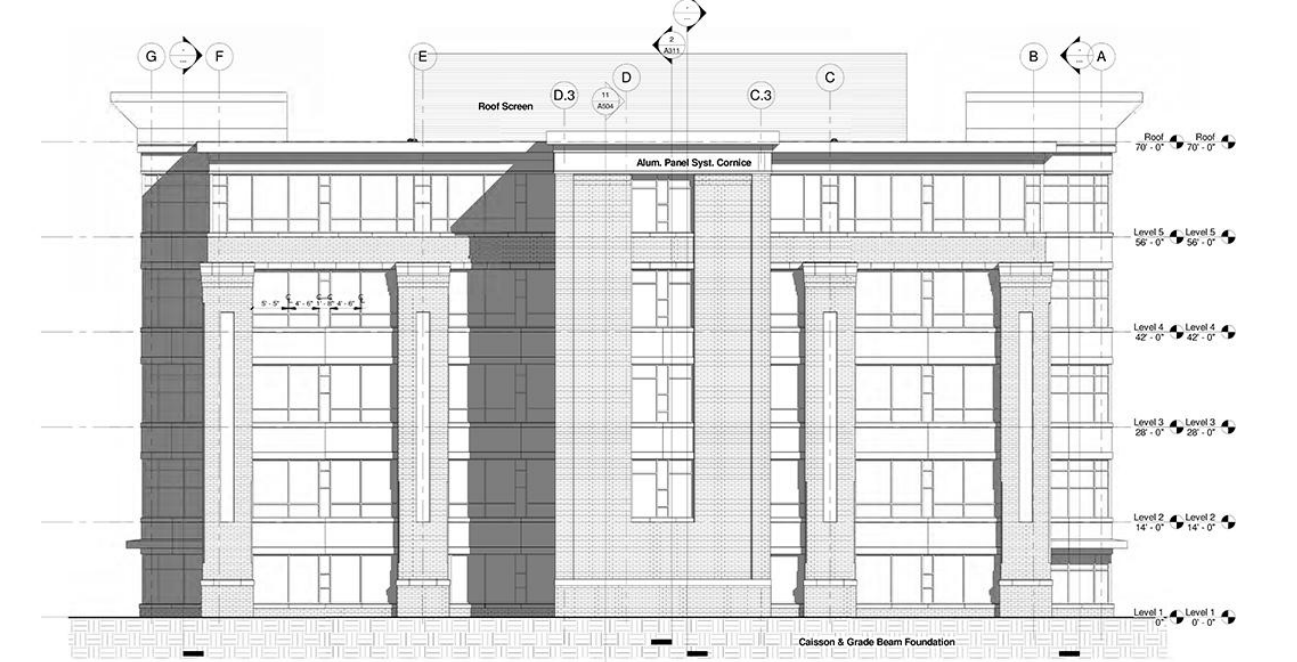




west



north



appendix



# glass type

6mm Dbl Low-E (e2=0.04) Tint 13 mm Argon

$$U = 0.233 \frac{BTU}{hr \cdot ft^2 \cdot ^\circ F}$$

shading coefficient = 0.32

